

SEABOARD GROUP II AND CITY OF HIGH POINT

July 1, 2013

Mr. Qu Qi, P.G.

North Carolina Department of Environment and Natural Resources
Division of Waste Management
1646 Mail Service Center
Raleigh, North Carolina 27699-1646

Report on Remedial Process Modifications at the Seaboard Group II and City of High Point Riverdale Drive Landfill Site in Jamestown, North Carolina

Dear Mr. Qi:

Seaboard Group II and the City of High Point (collectively herein the "Parties") provide you this report explaining the reasons for, and design of, the modifications to the remedial treatment system at the former Seaboard Chemical Corporation facility and closed Riverdale Drive Landfill (collectively herein the "Site"). The Remedial Action Pre-Construction Report for the mechanical treatment systems (PCR) was submitted to North Carolina Department of Environment and Natural Resources (NCDENR) on December 28, 2009. The report was subsequently approved by NCDENR, Division of Waste Management on March 22, 2010.

At this time, the remedial treatment systems at the Site, as described in the approved Pre-construction Report, has been installed and is operational. The automation and irrigation upgrades, as well as most other items that were known to be required for initial startup and testing, were complete during the first quarter of 2013. The Parties are currently in the process of revising, modifying and adding certain components due to unexpectedly high metals concentrations in the leachate.

Reasons for the Modifications

Recently it was determined that the levels of iron and magnesium in the leachate and groundwater were significantly higher during treatment system operation than those detected during earlier testing and used for the process design submitted in the PCR. Neither the advanced oxidation process (AOP⁺) system nor the phytoremediation system can tolerate the higher metals levels that would have resulted from the higher inlet concentrations to the existing system as proposed in the PCR. The existing Metals Removal Vat was not designed to handle the increase in metals loading. At first, this was thought to possibly be a temporary spike in metal concentrations due to initial system operations. However, was later determined to be an indication of an apparently chronic high level of metals, particularly in the leachate.

Once the system was started up after the automation and irrigation upgrades were complete, samples were collected from all of the leachate collection tanks and certain groundwater

observation wells at the Site. The samples were collected from each leachate tank, the Northern Intermittent Stream (NIS) Sump and Deep River Observation wells (OWDR) -1, OWDR-2, OWDR-3 and OWDR-4. The results of those analyses are presented in the following table.

Table 1 – Initial Sample Results

Parameter	OW-DR1	OW-DR2	OW-DR3	OW-DR4	LCHT-1	LCHT-2	LCHT-3	LCHT-4	LCHT-5	NIS SUMP	Comp	Average*
TDS	976	1030	1430	808	1320	2600	4700	3960	808	1100	2190	1902
TSS	4	26	2.5	4	220	98	36	226	56	94	123	80.86
Nitrate -N	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10	0.11	0.68	<0.10	0.33	0.26	0.3
Nitrite -N	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10	0.11	0.35	<0.10	0.20	<0.10	0.15
Iron, total	8.71	8.52	0.37	4.44	44.90	34.10	34.70	93.80	16.80	44.5	32.50	29.39
Total Mn	8.19	6.44	1.22	7.57	0.335	0.408	0.633	0.445	2.68	4.06	1.55	3.048
Total Mg	92.9	84.5	143.0	78.9	52.1	74.3	61.7	83.9	42.6	58.7	58.6	75.56
Total Na	44.8	43.4	27.5	45.1	197.0	512.0	932.0	853.0	85.2	151.0	404.0	299.55
pH, lab	NA	NA	NA	6.2	6.5	6.6	7.1	7.4	6.2	6.6	7.4	6.75
pH, field	6.6	7.7	6.1	7.3	7.1	7.3	7.5	7.8	7.3	7.5	7.9	7.28

The total metals concentrations in leachate tanks (LCHT) 1 through 5 and the Northern Intermittent Stream (NIS) sump during this sampling event were all considerable higher than the 10 mg/l expected from earlier sampling events such as those collected during the PhotoCat pilot study. The LCHT tanks and NIS sump iron levels averaged 44.8 mg/l of total iron, which is over four times what was anticipated in the system design included in the PCR. The reason for the increase is beyond the scope of this report and undetermined at this time; however, neither the PhotoCat system nor the phytoremediation system can tolerate metals at the determined concentrations.

Therefore, the Parties determined that the amount of sludge generated by this increase in average metals concentration would result in frequent stoppages of the process to remove the metals precipitate residues from the metals removal vat even if it could be modified to remove the metals to levels below the concentrations needed prior to final treatment. Therefore the Parties decided that modifications to the mechanical system to address the need to remove additional metals were required. The modifications are underway at this time and the progress is on schedule to conform to that approved in Technical Memorandum E-7. Once these modifications are complete, the Parties will resume startup testing by rerunning the initial alarm and interlock testing prior to beginning the planned drawdown test. At this time, the Parties believe, and are using best efforts, to be ready for full operation by January 1, 2014.

Modification Design

Pilot Testing

The initial step in the design of the modified process was to conduct a pilot study. The goal of the pilot study performed by the Parties in March and April 2013 was to attempt to determine the effects of fine bubble aeration, pH adjustment, filtration and settling on the combined leachate and groundwater flowing through the treatment system at various stages in the process. This included at the inlet to Lift Station (LS)-1, the inlet to LS-2 and at the outlet of the existing metals vat in the final treatment area.

In determining the most effective resolution to these problems, the Parties referred to work performed much earlier in the remedial action, in support of the Feasibility Study, by ERM-NC, PC. In a report authored by Dr. Richard Brown several methods of iron and other metals control were explored, including sequestration, chelation, ion exchange and aeration. The only method determined to be operationally and economically feasible at the Site was aeration.

In past testing, the concentrations of iron and other metals detected in the combined groundwater and leachate had been reported to be low. During the pilot testing of the advanced oxidation system (AOP), and other testing performed earlier, the concentration of iron, in particular, was indicated to be in the range of 10 to 20 mg/l. Recent testing has determined that, particularly in the leachate, the iron level is much higher, sometimes in the range of 100 to 120 mg/l and averaging approximately 45 mg/L. It was therefore concluded it would be necessary to address the iron and other metals in that process flow to avoid fouling of pipes and equipment. In addition, it would be necessary to remove most of the iron and other metals from the groundwater flow as it enters the system rather than in the main treatment structure to avoid fouling the pipes inside Lift Station 2 (LS-2) and the main treatment structure.

This seemed to require the system design be modified to add aeration at LS-1 and the installation of a new pretreatment process to include a larger filter and an air stripper system to process the combined flow of all groundwater and leachate prior to it entering the main treatment system. It was also determined that this will require a new building, because the floors installed in the existing structures were not capable of supporting the weight of the properly sized filter bodies once they were full of water.

Based upon this information a pilot study was scoped and performed to simulate a proposed process design. This modification would consist of aeration at LS-1, followed by aeration and filtration in a new portion of the pretreatment system prior to the combined flows entering LS-2 for final pretreatment before either being further processed by the AOP⁺ and discharged to the City of High Point Eastside Wastewater Treatment Plant, or used to irrigate the phytoremediation system on the closed Riverdale Drive Landfill cap.

Pilot Test Procedure

The Parties collected fresh samples of the leachate from the LCHT tanks and the NIS sump, as well as a sample of the groundwater from PWDR-1 (the primary groundwater pumping well), and the RWLFS wells for the purpose of performing design and pilot testing. These samples were composited by the Parties to roughly simulate the composition of the various inlet streams to the treatment system.

1. On March 11, 2013 the laboratory¹ received the following samples:
 - 3 liters of composite from the 6 leachate collection tanks (LCHT1-5, NIS Sump) that flow untreated into LS-1 as leachate; and
 - 3 liters of composite from RWLFS, NIS and the SIS wells which flow untreated into LS-1 as groundwater; and
 - 6 liters of composite from PWDR1 groundwater that flows untreated into the Metals Removal Vat and is the primary groundwater pumping well.

¹ Laboratory as used herein refers to Meritech, Inc. of Reidsville, NC, a NC certified laboratory.

2. Upon receipt the laboratory decanted the PWDR1 water for BOD₅, COD, TSS, TDS, Fe⁺⁺, Fe⁺⁺⁺, TOC, U.S. EPA Method 8260, and 1,4-dioxane testing. (Tracked internally at the laboratory as Sample #1, Initial Groundwater).
3. Also upon receipt, the composite of the leachate samples was combined with the RWLFS, NIS and SIS groundwater, at a ratio of 60% groundwater and 40% leachate to simulate the anticipated composition of the feed. That mixture was then poured off for BOD₅, COD, TSS, TDS, Fe⁺⁺, Fe⁺⁺⁺, TOC, U.S. EPA Method 8260, and 1,4-dioxane testing. (tracked internally at the laboratory as Sample #2).
4. On March 14, 2013 the laboratory split sample #2 into 3 sub-samples, and adjusted the pH of one sample to 7.5-8.0 (7.7 SU actual pH) with 0.2N NaOH (tracked internally at the laboratory as Stage 2 High pH Sample), one sample to 3.5-4.0 (3.5 SU actual pH) using 0.2 N H₂SO₄ (tracked internally at the laboratory as Stage 2 Low pH Sample), and left the third sample unchanged (7.0 SU actual pH, tracked internally at the laboratory as Stage 2 Unchanged pH Sample).
5. All three Stage 2 samples were then aerated with fine bubble diffusion for two hours using a 1" "airstone manifold apparatus" and an air pump.
6. After aeration, all three Stage 2 samples were allowed to settle for 2 hours.
7. Addition of the Iron Sulfate to the low pH sample to bring the total Iron concentration to approximately 50 mg/L was omitted because total Iron concentration in this mix was found to be higher than 50 mg/L (69.1 mg/L).
8. Stage 2 low pH sample was then titrated with 30% Hydrogen Peroxide at a ratio of 1 part iron per 25 parts hydrogen peroxide to simulate a Fenton's reagent reaction. (Amount was calculated to be 4.7 ml H₂O₂)
9. Stage 2 low pH sample was slowly mixed for 1 hour, while maintaining the pH between 3.5 and 4.0 (sample did not change pH).
10. The top part of the Stage 2 samples was poured off for the following tests: the high pH sample for parameters- BOD₅, COD, TSS, TDS, Fe⁺⁺, Fe⁺⁺⁺, TOC; the unchanged sample for parameters BOD₅, COD, TSS, TDS, Fe⁺⁺, Fe⁺⁺⁺, TOC; and the low pH sample for BOD₅, COD, TSS, TDS, Fe⁺⁺, Fe⁺⁺⁺, TOC, 8260, and 1,4-dioxane.
11. We then decanted liquid from all Stage 2 samples separately, mixing PWDR1 groundwater into each sample at a ratio of 60% PWDR1 and 40% sample solution, forming three separate Stage 3 samples.
12. All Stage 3 samples were aerated for two hours simulating the fine bubble diffusion again using the 1" airstone manifold apparatus and air pump.
13. After aeration all three samples were filtered through a 50-micron filter media and the filtrate was poured off to test for all parameters BOD, COD, TSS, TDS, Fe⁺⁺, Fe⁺⁺⁺, TOC, U.S. EPA Method 8260, and 1,4-dioxane.

The Parties determined that after the laboratory composited the PWR-1 and RWLFS and SIS samples and aerated the solution, there was little effect on BOD₅ and COD unless they lowered the pH. However at neutral and high pH they did show a marked reduction in iron. Both the unchanged and high pH samples were lower in iron than the low pH sample. Following that through to the Stage 3 sample results the laboratory indicated about the same final concentration whether or not they raised the pH. However, the concentration indicated was

well within the levels that can be managed in the Metals Removal Vat and tolerated by the downstream final treatment systems. See Attachment 1 for the laboratory report and results.

From these results it was determined that running at high pH is the best alternative but, the Parties are not certain why there was little or no reduction in iron indicated as a result of the initial aeration during Stage 2. Regardless of the need to reduce iron it was determined that aeration at the LS-1 inlet should be included in the modified process to eliminate the risks associated with the possibility of methane being present in the leachate. Aeration should also help remove some of the VOCs and cVOCs at that point, as well as help to maintain aerobic conditions regardless of the proportion of leachate mixed into the groundwater or the length of storage in the treatment tanks at LS-1.

Metals Removal Upgrade

The metals removal upgrade consists of adding an aeration tank to the flow path at LS-1. The aeration tank will employ ceramic fine bubble diffusers to aerate the combined leachate and groundwater flow exiting the inlet manifolds in LS-1. It was determined that all of the leachate and groundwater entering the system would be collected in a large (approximately 4,200 gallon) tank that is aerated by ceramic fine bubble diffusion. That tank will overflow into a surge tank inside LS-1 before it is pumped up to the existing LS-2. This piping exists and will simply be revised to direct the flow into the new "Filter Building."

It was determined the "Media Filters" would not adequately handle the flow anticipated. Further investigation determined that the main treatment structure floors would be unable to support filter bodies of the size needed for proper filtration. With properly sized filter bodies, the vessels were estimated to be 4 feet in diameter and 6 feet tall. In round numbers that meant the total weight of a single vessel would be approximately 7,000 pounds.

That lead to the decision the filters and associated equipment needed to be installed in a new 30 by 30 foot metal structure constructed on a concrete pad designed to support the filter bodies, and to provide aeration and filtration of the entire flow of groundwater and leachate prior to its entry into the main treatment structure.

The new Filter Building will receive the flow from LS-1 and mix it with the flow from PWDR-1 and certain SIS wells in an aerated tank to provide a relatively consistent 50 GPM. A vertical flat-bottomed tank with the fine bubble ceramic diffusers will be used for initial mixing and aeration. Aeration at this point will help reduce the VOC and cVOC loading on the air stripper influent thereby improving its efficiency, further oxidize metals and remove any remaining methane prior to it being further distributed throughout the building. The aeration tank will gravity overflow into an equalization tank before it is pumped through a set of 50-micron fixed bed filters designed to process 50 GPM. Those filters will be backwashed through another bag filter to capture the solids down to 50 micron with the liquid being returned to the system for further processing. Solids from the solids filter will be properly characterized and stored, handled and disposed in accordance with the North Carolina regulations.

Effluent from the filters will be sent to the six-tray air stripper which will be relocated to the Filter Building. Effluent from the air stripper will be pumped back into the main treatment structure through a newly installed 3" line inside of LS-2 which will discharge into the Metals

Removal Vat. The remaining process flow will be as described in the PCR. Attachment 2 to this report is a set of drawings showing the proposed revisions, and more detailed information.

Remedial Construction Work Remaining

Due to delays in acquiring the requisite building permit, work on the filtration building was delayed during the second quarter of 2013. All of the equipment with the exception of the tanks is at the site at this time.

The following activities remain to complete the construction and implementation of this modification:

Lift Station-1

Complete except for the installation of the aeration tank.

Lift Station-2

Complete except for the modifications for the filter building that are in progress.

Main Treatment Structure

Complete except for the modifications for the filter building that are in progress.

Filter Building

Building permits were applied for in April and were received on June 10, 2013. We are installing the grounding mat and concrete pad at this time and will proceed from there directly into pouring the pad and erecting the building.

Summary

The remedial activities are now on schedule to be completed by the date approved by NCDENR in TM E-7. Everything known to be necessary to begin the startup and testing of the system is either in the process of being installed, or has been completed, tested and is ready to be placed in service. The system startup testing will resume as soon as the filter building modifications are complete.

This system requires a phased startup in which each phase is followed by a series of tests which, when successfully completed, allows the system to progress to the next phase. The final phase is complete when the system is in full operation processing 50 gallons per minute (GPM) of combined leachate and groundwater. The testing is scheduled to be complete and the system ready for full operation on or about December 31, 2013.

Please contact Mr. Gary D. Babb (919-325-0696) or James C. LaRue (281-431-3571) if there are any questions or comments. Please direct correspondence related to this matter to:

Gary D. Babb, P.G.
Seaboard Group II and City of High Point
c/o Babb & Associates, P.A.
P.O. Box 37697
Raleigh, NC 27627.

Communications via electronic mail should be directed to gbabb@nc.rr.com and jarue@swenv.com.

Respectfully,

Seaboard Group II and City of High Point

The image shows two handwritten signatures in black ink. The signature on the left is for James C. LaRue, and the signature on the right is for Gary D. Babb. Both signatures are written in a cursive, flowing style.

James C. LaRue
Seaboard Group II

Gary D. Babb, P.G.
City of High Point

cc Amos Dawson, Esq. Counsel
Chris Thompson - City of High Point
Randy Smith - Seaboard Remediation Trust
Jackie Drummond – NCDENR

Attachment 1

Attachment 2

BUILDING SPECIFICATIONS

The manufacturer is not responsible for the concrete foundation design. The structure under this contract has been designed and detailed for the loads and conditions stipulated in the contract and shown on these drawings. Any alterations to the structural system or removal of any component parts, or the addition of other construction materials or loads must be done under the advice and direction of a registered architect, civil or structural engineer. The manufacturer will assume no responsibility for any loads not indicated.

This manufactured building is designed with the manufacturer's standard design practices which are based on pertinent procedures and recommendations of the following organizations and codes :

- American Institute of Steel Construction "Specification for the design fabrication and erection of structural steel for buildings" 13th edition.
- American Iron and Steel Institute "Specification for the design of cold formed steel structural members" 2007 edition.
- American Welding Society "Structural Welding Code" AWS D1.1
- Metal Building Manufacturers Association "Specification for the design fabrication and erection of the structural system" most current edition.

Material properties of steel plate and sheet used in fabrication of primary rigid frames and all primary structural framing members (other than cold-formed sections) conform to ASTM A-529 or A-572 all with a minimum yield point of 55 KSI.

Material properties of cold formed light gage steel members conform to the requirements of ASTM A-653, with a minimum yield point of 55 KSI

High strength bolts and their installation shall conform to ASTM specification A-325 and are designed as bearing type connections with threads included in the shear plane. All high strength bolts are to be installed to the "Snug-Tight" condition as defined by the RSCS Specification for Structural Joints Using A325 or A490 Bolts, 2004 Edition, section 8.1, unless noted otherwise. Crane Building's Rigid Frame shall be installed in accordance with "Turn-of-Nut Pretensioning" per section 8.2.1. Bolts in standard holes do not require washers per section 6.

All primary structural members except bolts and fasteners shall receive one coat of Iron Oxide inhibitive primer.

Shop and field inspections and associated fees are the responsibility of the contractor, unless stipulated otherwise.

CONTRACTOR RESPONSIBILITIES

The contractor must secure all required approvals and permits from the appropriate agency as required.

Approval of the manufacturer's drawings and calculations indicate that the manufacturer has correctly interpreted and applied the requirements of the contract drawings and specifications. (AISC 303-05 Code of Standard Practice)

Where discrepancies exist between the manufacturer's structural steel plans and the plans for other trades, the structural steel plans shall govern. (Section 3.3 AISC 303-05 Code of Standard Practice)

Design considerations of any materials in the structure which are not furnished by the manufacturer, are the responsibility of the contractor and engineers other than the manufacturer's engineering, unless specifically indicated.

The contractor is responsible for all erection of steel and associated work in compliance with the manufacturer's "For Construction" drawings.

Temporary supports, such as guys, braces, flashwork or other elements required for the erection will be determined and furnished and installed by the erector. (Section 7 AISC 303-05 Code of Standard Practice)

It is the contractor's responsibility to apply or observe all pertinent safety rules and regulations, as per OSHA standards as applicable.

The Contractor is responsible for the verification of all shipments received. Any "external" damage or shortages must be noted on all copies of the bill of lading and one copy is to be retained for your records. Failure to do so will make it impossible for the factory to honor any claim. NO EXCEPTIONS!!!

BISON STEEL BUILDINGS, INC.



DESIGN LOADING

This structure is designed utilizing the loads indicated and applied by the :
NCBC 2012

It is the contractor's responsibility to confirm that these loads comply with the requirements of the local building department.

Specific loads : (See structural calculations and foundation reactions.)

- 20 PSF Live Load
- LL Reduction Allowed : Yes No
- 15 PSF Ground Snow Load
- 1.2 Thermal Factor (Ct)
- 1.0 Snow Exposure Factor (Ce)
- 90 MPH Wind Load Exposure B (If applicable)
- 2.2 PSF Dead Load (Metal Bldg. Weight - Purlins, Panels, Etc.)
- 1 PSF Collateral Load
- II Occupancy Category (I_v= 1.00 I_s= 1.00 I_e= 1.00)

DRAWING INDEX

- CS-1 Drawings Cover Sheet
- CS-2 Fastener Schedule
- E1 Anchor Bolt Plan
- E2 Anchor Bolt Details & Reactions
- E3 Rigid Frame Elevation
- E4 Sidewall Framing
- E5 Endwall Framing
- E6 Roof Framing & Sheeting
- E7 Sidewall Sheeting
- E8 Endwall Sheeting
- E9 Detail Drawings
- E10 Detail Drawings
- E11 Detail Drawings
- E12 Trim Drawings

SEISMIC DATA :

- 1) Mapped Spectral Acceleration for Short Period, S_s 0.218
- 2) Site Coefficient, F_a 1.60
- 3) Seismic Design Category = B
- 4) Site Class = D
- 5) Basic Structural System and Seismic Resisting System
Ordinary Moment Frame of Steel
- 6) Frames: R = 3.00
- 7) Cables: R = 3.00
- 8) Analysis Procedure = Equivalent Lateral Force

These Drawings are for :

- Construction Approval *
 - Permit Anchor Bolts & Reactions
- * Approval orders must be released for fabrication within thirty (30) calendar days after the submittal drawings are issued or they will be subject to any current price increases. Special attention should be given in approving dimensions and/or details. Please verify requested dimensions by indicating 'OK'.

Building is manufactured by STEEL BUILT CORPORATION. STEEL BUILT CORPORATION is a fabricator approved by the following agencies.

1. QUASAR/CWB GROUP - CAN/CSA A660 Certificate # STEBUO
2. INTERNATIONAL ACCREDITATION SERVICE, INC.
Fabricator Inspection Program FA - 446
3. City of Houston Approved Fabricator Registration Number - 759
4. City of LA Approved Fabricator
Type I FABRICATOR LICENSE NUMBER - #2091

Engineering Seal

This certification covers parts manufactured and delivered by the manufacturer only, and excludes parts such as doors, windows, foundation design and erection of the building.

DSN: DAZ	DWN: HTS	REV:	DRAWINGS COVER SHEET		
DET:	CHK:	REVISIONS			
		NO.	DATE	CUSTOMER : SEABOARD REMEDIAL ACTION TRUST FUND GREENSBORO, NC GUILFORD COUNTY BISON STEEL BUILDINGS, INC. 2619 COON RAPIDS BLVD NW MINNEAPOLIS, MN	
PROFESSIONAL ENGINEER		SCALE: NOT TO SCALE	DATE: 3/18/13	JOB NO: 16927	SHT. NO: CS-1

NOTICE

Be advised that all shipments are via outside trucking companies and are signed for in good condition and completeness at the pick-up location by the driver.

"No claim will be honored" unless the following procedures have been followed:

AT TIME OF RECEIPT: At the delivery point the driver is required to provide you with a bill of lading which lists and illustrates all bulk items to be received. Any "external" damage or shortage must be noted on all copies of the bill of lading and one copy is to be retained for your records. Failure to do so will make it impossible for the factory to honor any claim.

NO EXCEPTIONS!!!

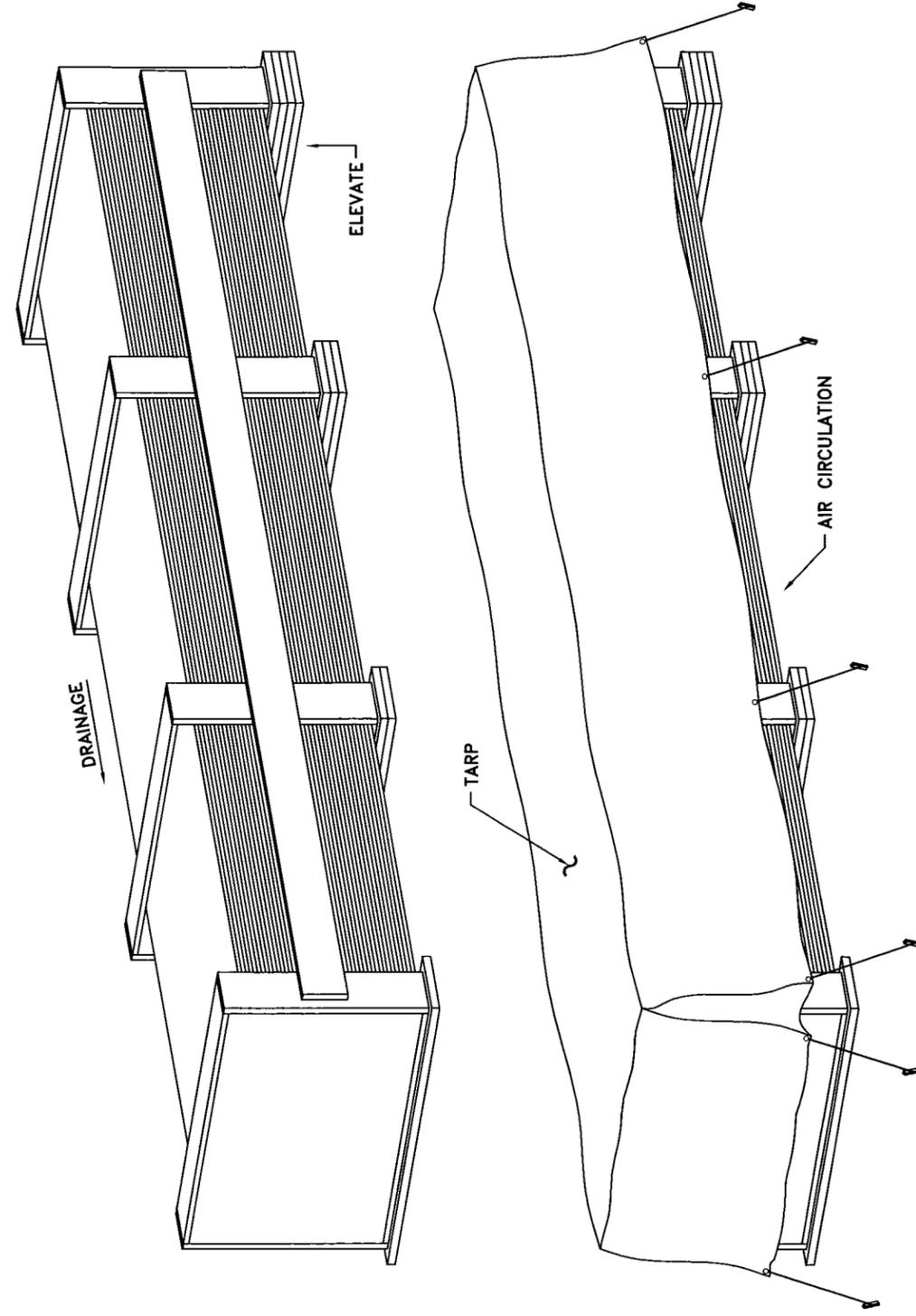
CUSTOMERS DETAILED INVENTORY CHECK:
(SHAKE-OUT)
It is a factory required policy that the customer receives a detailed shipping list (packing list) that specifies all included quantities of individual parts. Valid concealed shortages must be reported to the factory within Valid 30 calendar days NO EXCEPTIONS!!!
The driver does not have to be present for your inventory confirmation.

SPECIAL NOTE #1:
Overhead doors, windows and service doors are shipped in cardboard boxes. It is required that they be opened to insure that the trucker's chains have not damaged the edges. If so, it must be noted on the bill of lading.

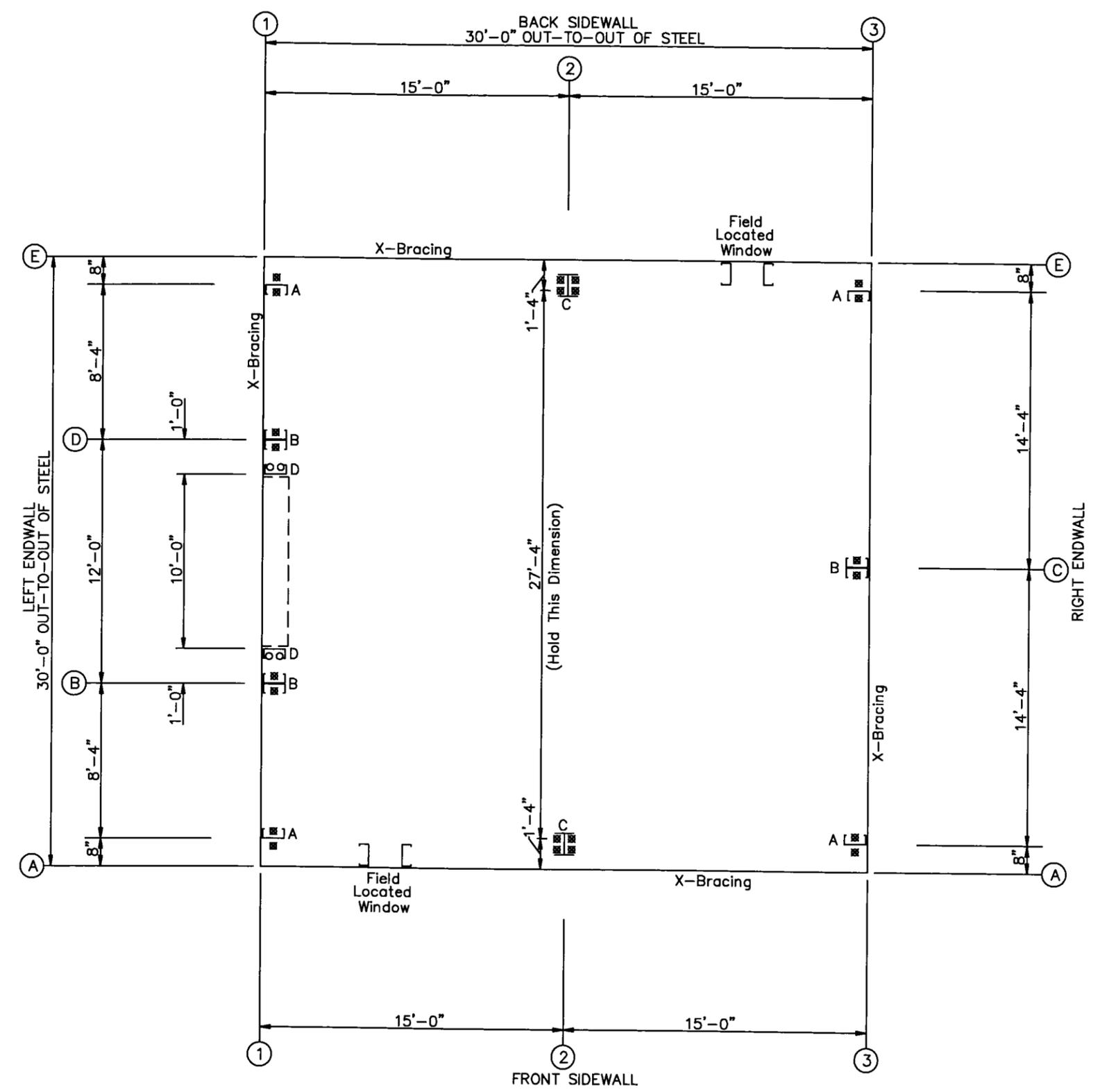
SPECIAL NOTE #2:
PERMIT DRAWINGS are NOT to be used for construction purposes. Dimensions and details on permit drawings may vary with construction drawings. Use construction drawings ONLY for the erection of your building.

NOTICE

If water is allowed to remain on or in bundles of painted or coated parts for extended periods of time, degradation will occur. The end result is shorter material life due to corrosion. Therefore, upon receipt of a job, all bundles of primed parts should be stored at an angle to allow any trapped water to drain away and permit air circulation for drying. Separate the panels to allow air to circulate between each panel. If environmental conditions are such, tarps should be used to protect materials. Puddles of water should not be allowed to collect and remain on columns or rafters for the same reason.

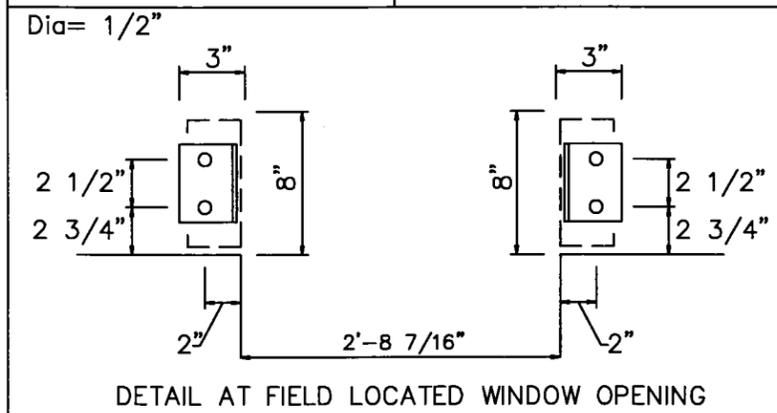
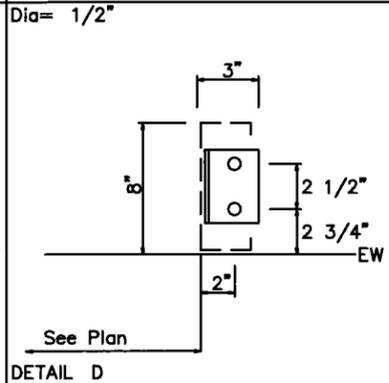
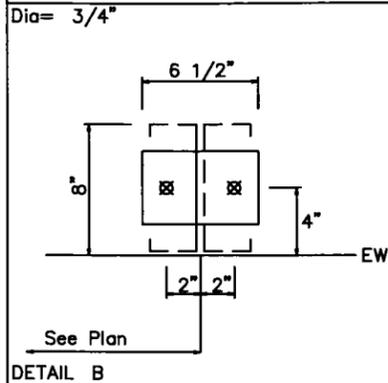
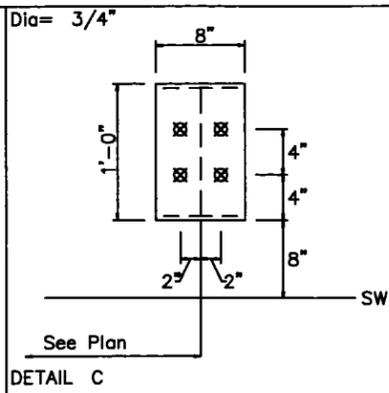
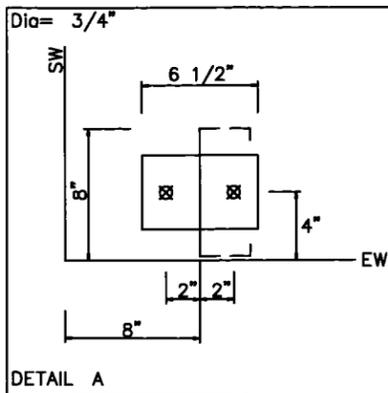


○ Dia= 1/2"
 ■ Dia= 3/4"



ANCHOR BOLT PLAN
 NOTE: All Base Plates @ 100'-0" (U.N.)

BISON STEEL BUILDINGS, INC.		SEABOARD REMEDIAL ACTION TRUST FUND	
City: MINNEAPOLIS	State: MN	City: GREENSBORO	State: NC
Designer: DAZ	Date: 3/18/13	Drafter: HTS	Date: 3/18/13
Detailer:	Date:	Office:	Job No.:
Checker:	Date:	Office:	16927
ANCHOR BOLT PLAN			Sht. E1 of 12



NOTES FOR REACTIONS

Building reactions are based on the following building data:

- Width (ft) = 30
- Length (ft) = 30
- Eave Height (ft) = 10 / 10
- Roof Slope = 4.0:12 / 4.0:12
- Dead Load (psf) = 2.200
- Collateral Load (psf) = 1
- Roof Live Load (psf) = 20.00
- Roof Snow Load (psf) = 12.6
- Wind Speed (mph) = 90
- Wind Code = NCBC 2012
- Wind Exposure = B
- Closed/Open = Closed
- Importance - Wind = 1.00
- Importance - Seismic = 1.00
- Seismic Design Category = B
- Seismic Coeff (Fa/Ss) = 0.349

Load Combinations

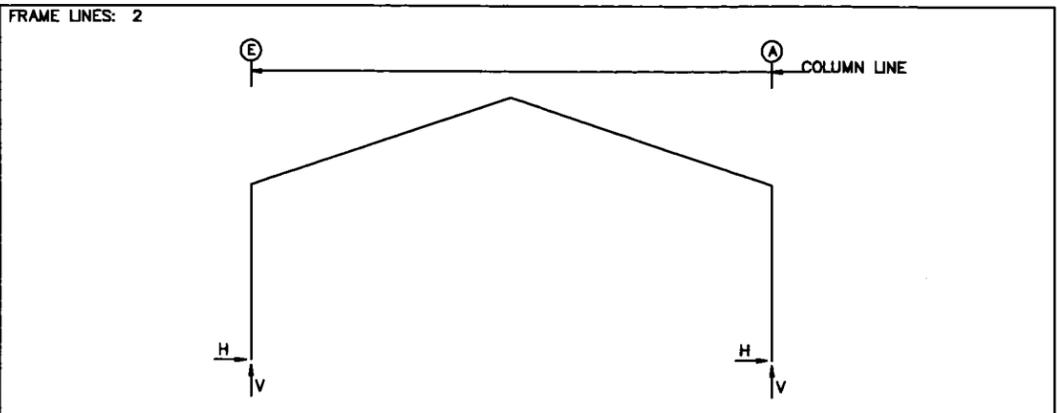
- DL+CL+(LL or SL)
- DL+CL+W
- DL+CL+0.75WL+0.75(LL or SL)
- DL+0.75(0.7SEIS)+0.75(LL or SL)
- 0.6DL+W
- 0.6DL+0.7SEIS

GENERAL NOTES

- FOUNDATION DESIGN AND CONSTRUCTION ARE NOT THE RESPONSIBILITY OF THE BUILDING MANUFACTURER.
- THE BUILDING REACTION DATA REPORTS THE LOADS WHICH THIS BUILDING PLACES ON THE FOUNDATION.
- THE SPECIFIED ANCHOR BOLT DIAMETER ASSUMES ASTM A307. ANCHOR BOLT MATERIAL OF EQUAL DIAMETER MEETING OR EXCEEDING THE STRENGTH REQUIREMENTS SET FORTH ON THESE DRAWINGS MAY BE UTILIZED AT THE DISCRETION OF THE FOUNDATION DESIGN ENGINEER.
- ANCHOR BOLTS TO BE SUPPLIED BY OTHERS. ANCHOR BOLT EMBEDMENT LENGTH SHALL BE DETERMINED BY THE FOUNDATION ENGINEER.
- ANCHOR BOLT PROJECTION ABOVE CONCRETE FINISHED SURFACE TO BE 3" UNLESS OTHERWISE NOTED BY FOUNDATION DESIGNER.
- ANCHOR BOLTS SHALL BE ACCURATELY SET TO A TOLERANCE OF +/- 1/8" IN ELEVATION AND LOCATION.
- THE ANCHOR BOLT LOCATIONS PROVIDED BY THE METAL BUILDING MANUFACTURER MAY NOT SATISFY ANCHOR BOLT CONCRETE EDGE DISTANCE REQUIREMENTS DEPENDING ON THE DETAILS OF FOUNDATION DESIGN. IT IS THE RESPONSIBILITY OF THE FOUNDATION DESIGN ENGINEER TO MAKE SURE THAT SUFFICIENT CONCRETE EDGE DISTANCE IS PROVIDED IN THE FOUNDATION DESIGN.
- MINOR FIELD WORK OF STRUCTURAL SECONDARY AND PANEL/TRIM ITEMS MAY BE NECESSARY TO ENSURE PROPER FIT. SUCH WORK IS CONSIDERED A NORMAL PART OF METAL BUILDING ERECTION. WE WILL NOT HONOR BACKCHARGES FOR MINOR FIELD WORK.
- THIS DRAWING IS NOT TO SCALE.

BUILDING BRACING REACTIONS

Wall Loc	Col Line	E.D	± Reactions (k)				Panel Shear (lb/ft)	
			Wind Horz	Wind Vert	Seismic Horz	Seismic Vert	Wind	Seis
L_EW	1	E,D	0.8	1.1	0.2	0.2		
F_SW	A	2,3	0.9	0.5	0.3	0.2		
R_EW	3	A,C	0.8	0.7	0.2	0.1		
B_SW	E	2,1	0.9	0.5	0.3	0.2		



RIGID FRAME: ANCHOR BOLTS & BASE PLATES

Frm Line	Col Line	Anc. Bolt Qty	Anc. Bolt Dia	Base Plate Width (in)	Base Plate Length (in)	Base Plate Thick (in)	Grout (in)
2	E	4	0.750	8.000	12.00	0.500	0.0
2	A	4	0.750	8.000	12.00	0.500	0.0

RIGID FRAME: BASIC COLUMN REACTIONS (k)

Frame Line	Column Line	Dead		Collateral		Live		Snow		Wind_Left1		Wind_Right1	
		Horz	Vert	Horz	Vert	Horz	Vert	Horz	Vert	Horz	Vert	Horz	Vert
2	E	0.3	1.0	0.1	0.3	1.4	4.2	1.2	3.5	-2.0	-3.3	0.8	-2.0
2	A	-0.3	1.0	-0.1	0.3	-1.4	4.2	-1.2	3.5	-0.8	-2.0	2.0	-3.3

Frame Line	Column Line	Wind_Left2		Wind_Right2		Wind_Long1		Wind_Long2		Seismic_Left		Seismic_Right	
		Horz	Vert	Horz	Vert	Horz	Vert	Horz	Vert	Horz	Vert	Horz	Vert
2	E	-2.2	-2.0	0.6	-0.7	-0.2	-3.5	-0.2	-2.3	-0.1	-0.1	0.1	0.1
2	A	-0.6	-0.7	2.2	-2.0	0.2	-3.5	0.2	-2.3	-0.1	0.1	0.1	-0.1

Frame Line	Column Line	Seismic_Long		F1UNB_SL_L		F1UNB_SL_R	
		Horz	Vert	Horz	Vert	Horz	Vert
2	E	0.0	-0.5	1.1	3.7	1.1	2.2
2	A	0.0	-0.5	-1.1	2.2	-1.1	3.7

ENDWALL COLUMN: BASIC COLUMN REACTIONS (k)

Frm Line	Col Line	Dead Vert	Collat Vert	Live Vert	Snow Vert	Wind_Left1		Wind_Right1		Wind_Left2		Wind_Right2		Wind Press Horz
						Horz	Vert	Horz	Vert	Horz	Vert	Horz	Vert	
1	E	0.1	0.0	0.4	0.2	0.4	-1.0	0.0	0.4	0.8	-1.5	0.0	0.9	-0.2
1	D	0.4	0.1	1.9	1.2	0.0	-0.5	0.4	-1.5	0.0	0.0	0.8	-2.1	-0.7
1	B	0.4	0.1	1.9	1.2	0.0	-0.7	0.0	-1.2	0.0	-0.5	0.0	-1.3	-0.7
1	A	0.1	0.0	0.4	0.2	0.0	-0.5	0.0	-0.3	0.0	-0.6	0.0	-0.2	-0.2

Frm Line	Col Line	Wind Suct Horz	Wind Long1 Vert	Wind Long2 Vert	Seis_Left		Seis_Right		E1UNB_SL_L		E1UNB_SL_R	
					Horz	Vert	Horz	Vert	Horz	Vert	Horz	Vert
1	E	0.3	-0.3	-0.2	0.5	-0.7	0.0	0.9	0.0	0.2	0.0	-0.1
1	D	0.8	-0.9	-0.5	0.0	0.7	-0.9	0.0	1.6	0.0	0.7	
1	B	0.8	-0.9	-0.5	0.0	0.1	0.0	-0.1	0.0	0.7	0.0	1.6
1	A	0.3	-0.3	-0.2	0.0	-0.1	0.0	0.1	0.0	-0.1	0.0	0.2

Frm Line	Col Line	Dead Vert	Collat Vert	Live Vert	Snow Vert	Wind_Left1		Wind_Right1		Wind_Left2		Wind_Right2		Wind Press Horz
						Horz	Vert	Horz	Vert	Horz	Vert	Horz	Vert	
3	A	0.2	0.1	1.2	0.7	0.4	-1.2	0.0	-0.2	0.8	-1.5	0.0	0.2	-0.4
3	C	0.4	0.1	2.2	1.4	0.0	-0.7	0.4	-1.6	0.0	-0.3	0.8	-2.0	-1.1
3	E	0.2	0.1	1.2	0.7	0.0	-0.7	0.0	-0.8	0.0	-0.8	0.0	-0.8	-0.4

Frm Line	Col Line	Wind Suct Horz	Wind Long1 Vert	Wind Long2 Vert	Seis_Left		Seis_Right		E2UNB_SL_L		E2UNB_SL_R	
					Horz	Vert	Horz	Vert	Horz	Vert	Horz	Vert
3	A	0.5	-0.7	-0.4	0.5	-0.4	0.0	0.6	0.0	0.8	0.0	0.2
3	C	1.2	-1.0	-0.6	0.0	0.4	0.5	-0.6	0.0	1.3	0.0	1.3
3	E	0.5	-0.7	-0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.8

ENDWALL COLUMN: ANCHOR BOLTS & BASE PLATES

Frm Line	Col Line	Anc. Bolt Qty	Anc. Bolt Dia	Base Plate Width (in)	Base Plate Length (in)	Base Plate Thick (in)	Grout (in)
1	E	2	0.750	6.500	6.000	0.188	0.0
1	D	2	0.750	6.500	6.000	0.188	0.0
1	B	2	0.750	6.500	6.000	0.188	0.0
1	A	2	0.750	6.500	6.000	0.188	0.0
3	A	2	0.750	6.500	6.000	0.188	0.0
3	C	2	0.750	6.500	6.000	0.188	0.0
3	E	2	0.750	6.500	6.000	0.188	0.0

LOAD CASES

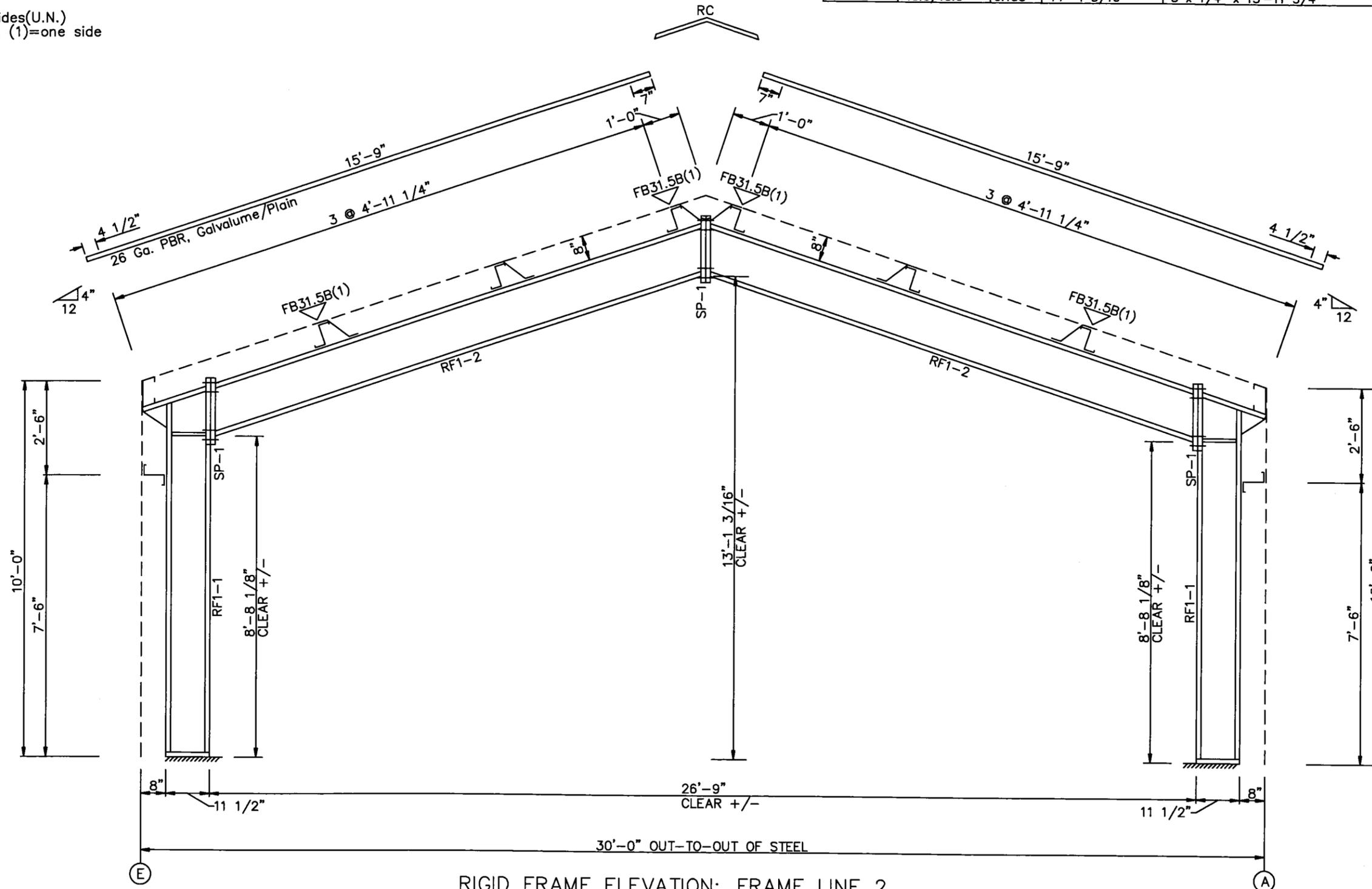
WIND_L1 = WIND LOAD FROM LEFT CASE 1
WIND_R1 = WIND LOAD FROM RIGHT CASE 1
WIND_LN1 = LONGITUDINAL WIND CASE 1
SEISMIC_L = SEISMIC LOAD FROM LEFT
SEISMIC_R = SEISMIC LOAD FROM RIGHT
SEISMICLN = LONGITUDINAL SEISMIC LOAD
F1UNB_SL_L = FRAME 1 UNBALANCED SNOW LEFT SIDE
F1UNB_SL_R = FRAME 1 UNBALANCED SNOW RIGHT SIDE
F1CRANE 1 = FRAME 1 CRANE LOAD IN POSITION 1
DRIFT = SNOW DRIFT LOAD
SLIDE = SLIDE SNOW LOAD

BISON STEEL BUILDINGS, INC.		SEABOARD REMEDIAL ACTION TRUST FUND	
City: MINNEAPOLIS	State: MN	City: GREENSBORO	State: NC
Designer: DAZ	Date: 3/18/13	Drafter: HTS	Date: 3/18/13
Detailer:	Date:	Office:	Job No.:
Checker:	Date:	Office:	16927
ANCHOR BOLT DETAILS & REACTIONS			Sht. E2 of 12

SPLICE BOLT TABLE						
Mark	Qty		Int	Type	Dia	Length
	Top	Bot				
SP-1	4	4	0	A325T	0.625	2.25

MEMBER TABLE						
Mark	Web Depth		Web Plate		Outside Flange	Inside Flange
	Start/End	Thick	Length	Thick	W x Thk x Length	W x Thk x Length
RF1-1	11.0/11.0	0.135	9'-9 1/4"		5" x 1/4" x 9'-5 1/2"	5" x 1/4" x 8'-3 13/16"
RF1-2	13.0/13.0	0.135	14'-4 3/16"		5" x 1/4" x 1'-8 3/16"	5" x 1/4" x 13'-11 3/4"

FLANGE BRACES: Both Sides(U.N.)
 FBxxB(1): xx=length(in), (1)=one side
 B - L2X2X1/8



RIGID FRAME ELEVATION: FRAME LINE 2

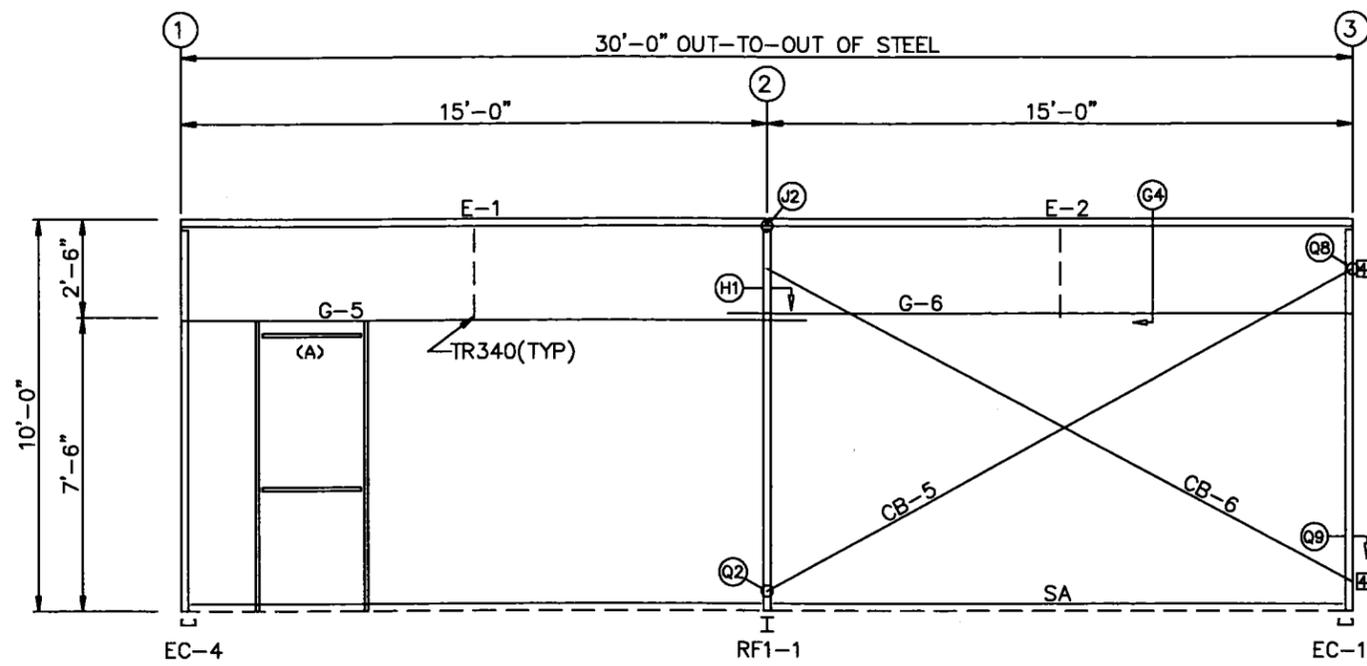
GENERAL NOTES:

MINOR FIELD WORK OF STRUCTURAL, SECONDARY AND PANEL/TRIM ITEMS MAY BE NECESSARY TO ENSURE PROPER FIT. SUCH WORK IS CONSIDERED A NORMAL PART OF METAL BUILDING ERECTION. WE WILL NOT HONOR BACKCHARGES FOR MINOR FIELD WORK.

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Checker:	Date:	Office:	16927
RIGID FRAME ELEVATION			Sht. E3 of 12

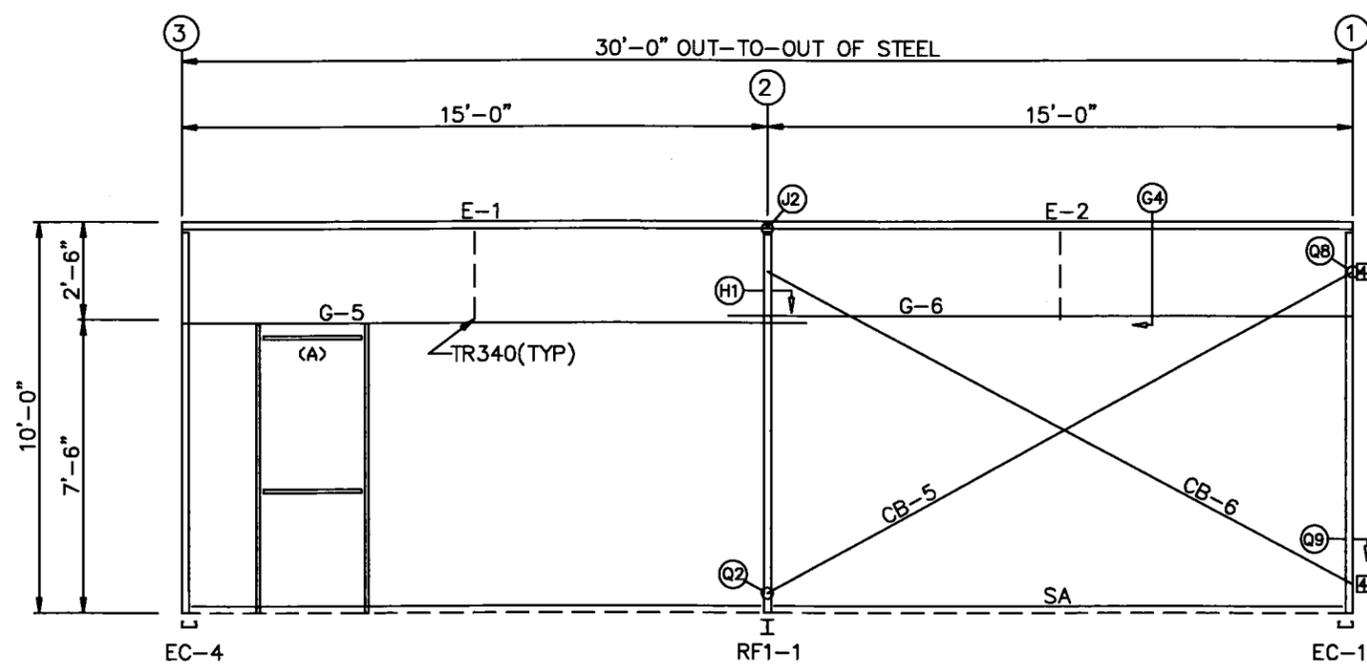
MEMBER TABLE FRAME LINE A & E		
MARK	PART	LENGTH
DJ-2	8x25C16	7'-1 1/2"
DH-2	8x25C16	2'-7 15/16"
DS-1	8x25C16	2'-7 15/16"
E-1	8x30E16	14'-11 1/4"
E-2	8x30E16	14'-11 1/4"
G-5	8x25Z16	15'-11 1/2"
G-6	8x25Z16	15'-11 1/2"
CB-5	0.25_CBL	14'-5"
CB-6	0.25_CBL	14'-10"

CONNECTION PLATES FRAME LINE A & E	
ID	MARK/PART
1	CLO02
2	CLO21
3	CLO25
4	CL253



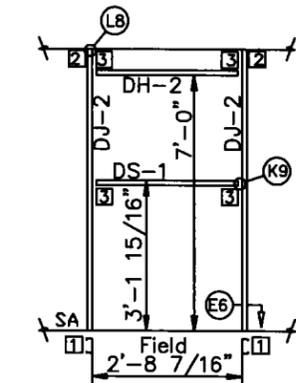
GIRT LAPS

SIDEWALL FRAMING: FRAME LINE A



GIRT LAPS

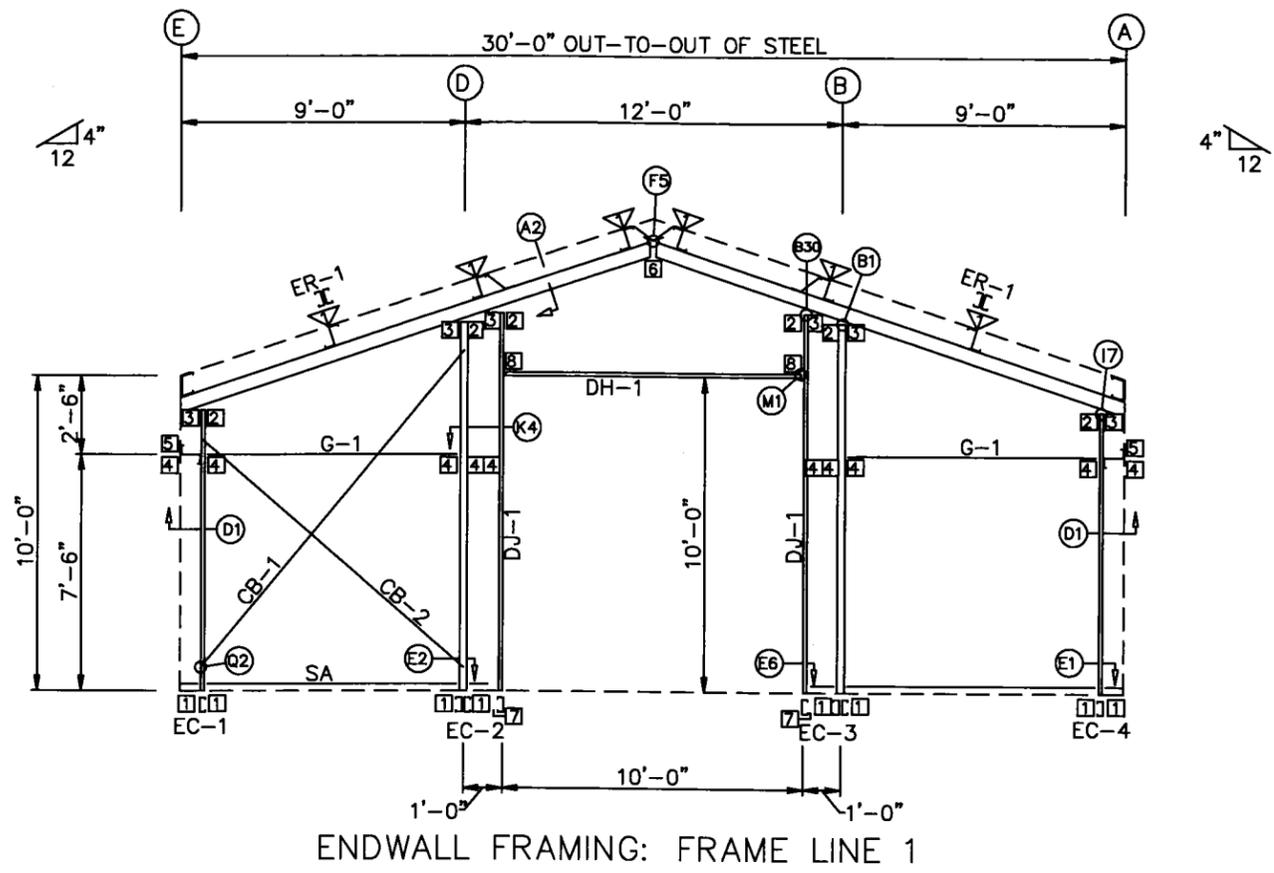
SIDEWALL FRAMING: FRAME LINE E



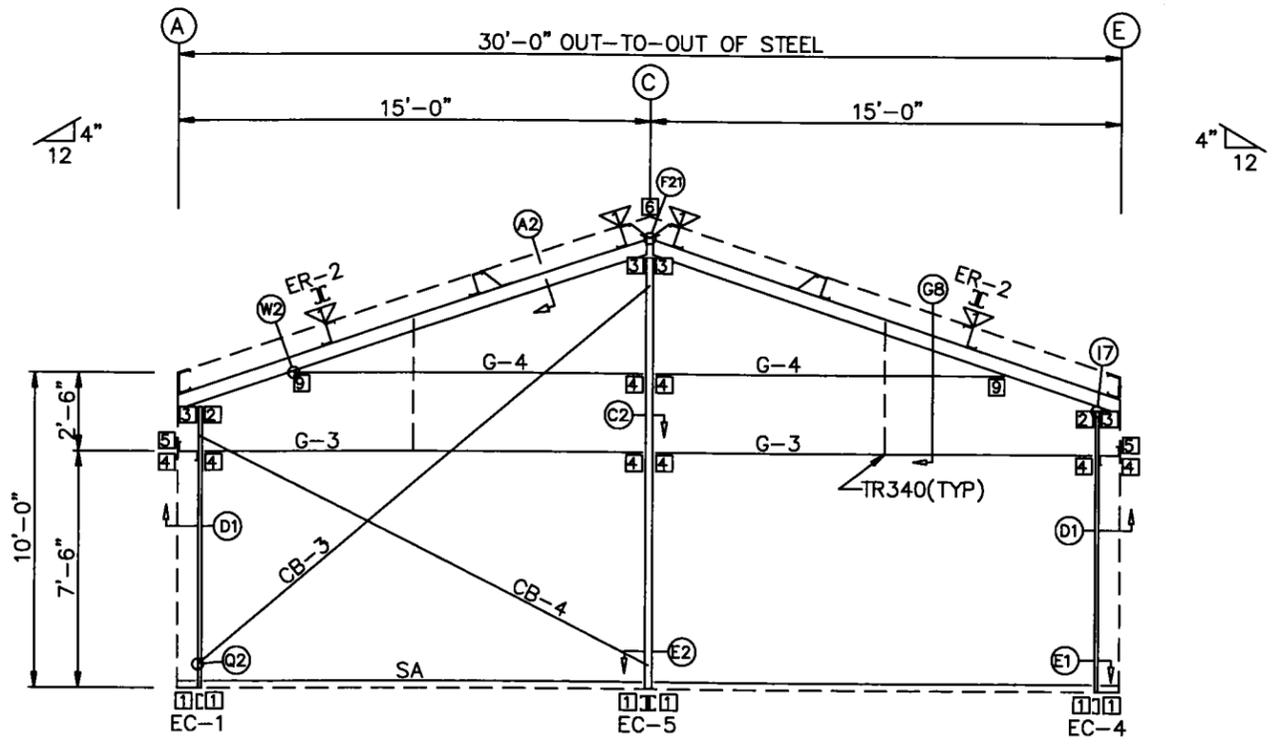
FRAMING REQ'D. FOR 2'-8 7/16" x 3'-10 1/16" FRAMED
OPENING FOR WINDOW
(2 REQ'D.)
(A)

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Checker:	Date:	Office:	16927
SIDEWALL FRAMING			Sht. E4 of 12



ENDWALL FRAMING: FRAME LINE 1



ENDWALL FRAMING: FRAME LINE 3

BOLT TABLE				
FRAME LINE 1 & 3				
LOCATION	QUAN	TYPE	DIA	LENGTH
ER-1/ER-1	4	A325T	1/2"	2"
ER-2/ER-2	4	A325T	1/2"	2"
Columns/Raf	8	A325T	1/2"	2"
Jamb	6	A325T	1/2"	2"

MEMBER TABLE		
FRAME LINE 1 & 3		
MARK	PART	LENGTH
EC-1	8x25C16	8'-8 13/16"
EC-2	8X50D15	11'-6 1/8"
EC-3	8X50D15	11'-6 1/8"
EC-4	8x25C16	8'-8 13/16"
EC-5	8X50D15	13'-6 1/8"
ER-1	8X50D15	15'-6 15/16"
ER-2	8X50D15	15'-6 15/16"
DJ-1	8x25C16	11'-10 1/8"
DH-1	8x25C16	9'-11 1/2"
G-1	8x25Z16	7'-7"
G-3	8x25Z16	13'-7"
G-4	8x25Z16	9'-10 15/16"
CB-1	0.25_CBL	11'-3"
CB-2	0.25_CBL	9'-3"
CB-3	0.25_CBL	16'-11"
CB-4	0.25_CBL	14'-4"

FLANGE BRACE TABLE		
FRAME LINE 1 & 3		
VID	MARK	LENGTH
1	FB28.8	2'-4 3/4"

CONNECTION PLATES	
FRAME LINE 1 & 3	
ID	MARK/PART
1	CLO03
2	CLO81
3	CLO83
4	CLO20
5	CLO50
6	CL122
7	CLO02
8	CLO25
9	CLO30

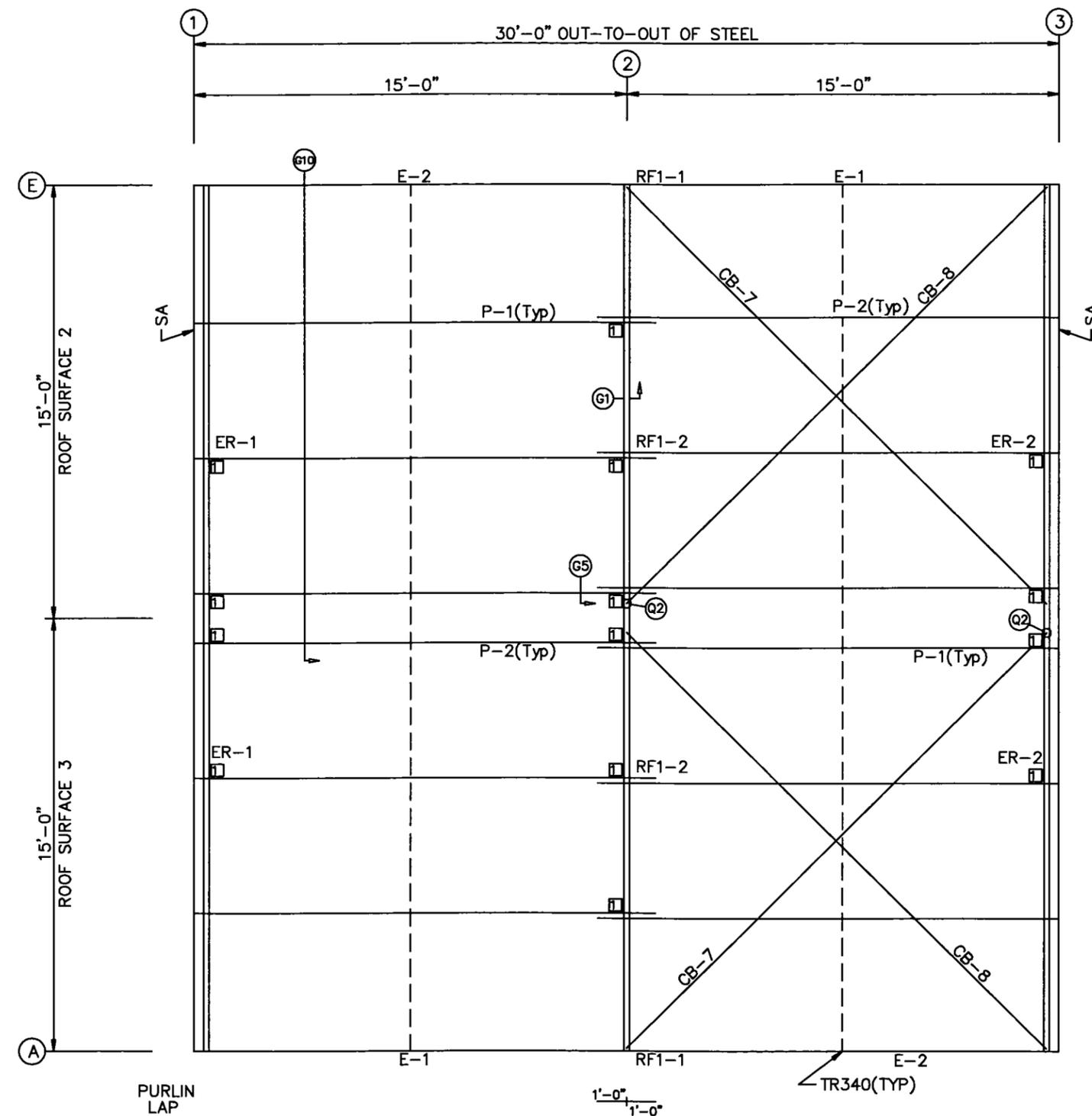
CABLE NOTES:
FIELD SLOT GIRTS FOR
CABLE TO PASS-THRU.

GENERAL NOTES:
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Detailer:	Date:	Office:	Job No.:
Checker:	Date:	Office:	16927
ENDWALL FRAMING			Sht. E5 of 12

MEMBER TABLE		
ROOF PLAN		
MARK	PART	LENGTH
P-1	8x25Z16	15'-11 1/2"
P-2	8x25Z16	15'-11 1/2"
E-1	8x30E16	14'-11 1/4"
E-2	8x30E16	14'-11 1/4"
CB-7	0.25_CBL	18'-7"
CB-8	0.25_CBL	19'-1"

CONNECTION PLATES	
ROOF PLAN	
ID	MARK/PART
1	CL156



ROOF FRAMING PLAN



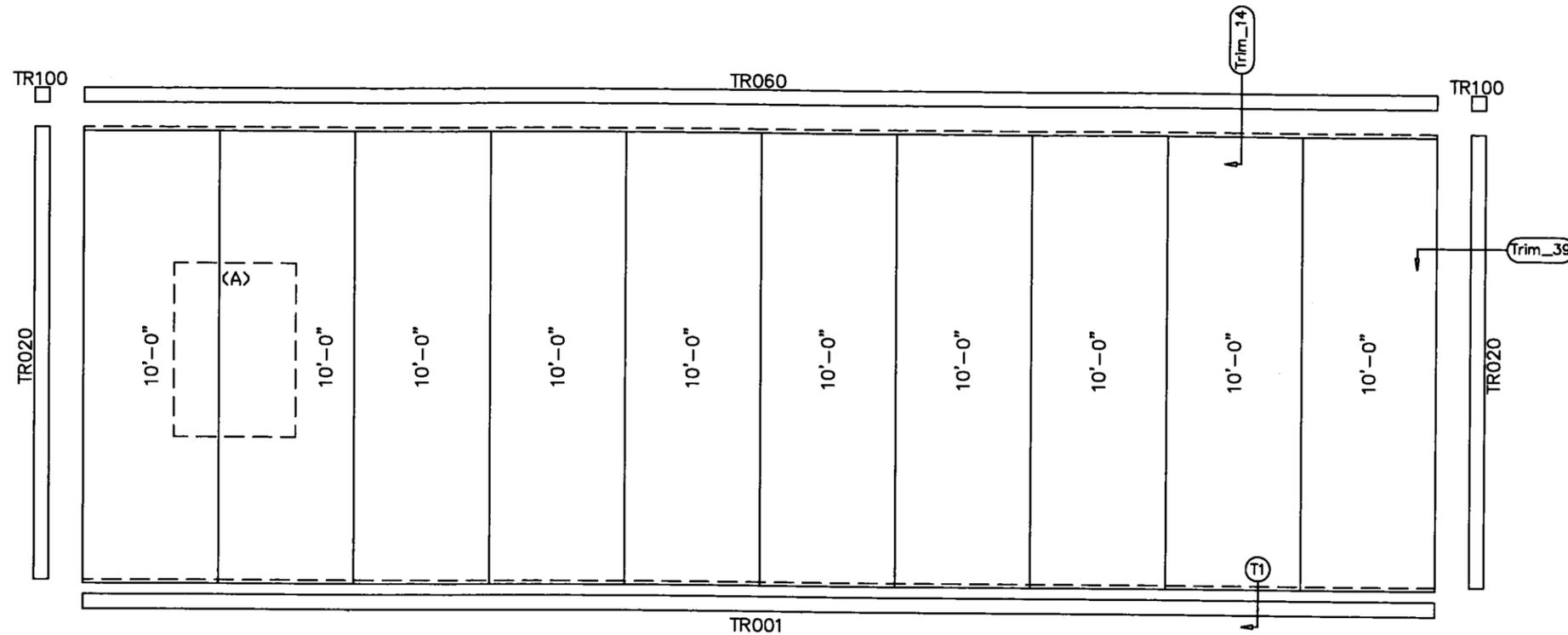
ROOF SHEETING

PANELS: 26 Ga. PBR Galvalume/Plain

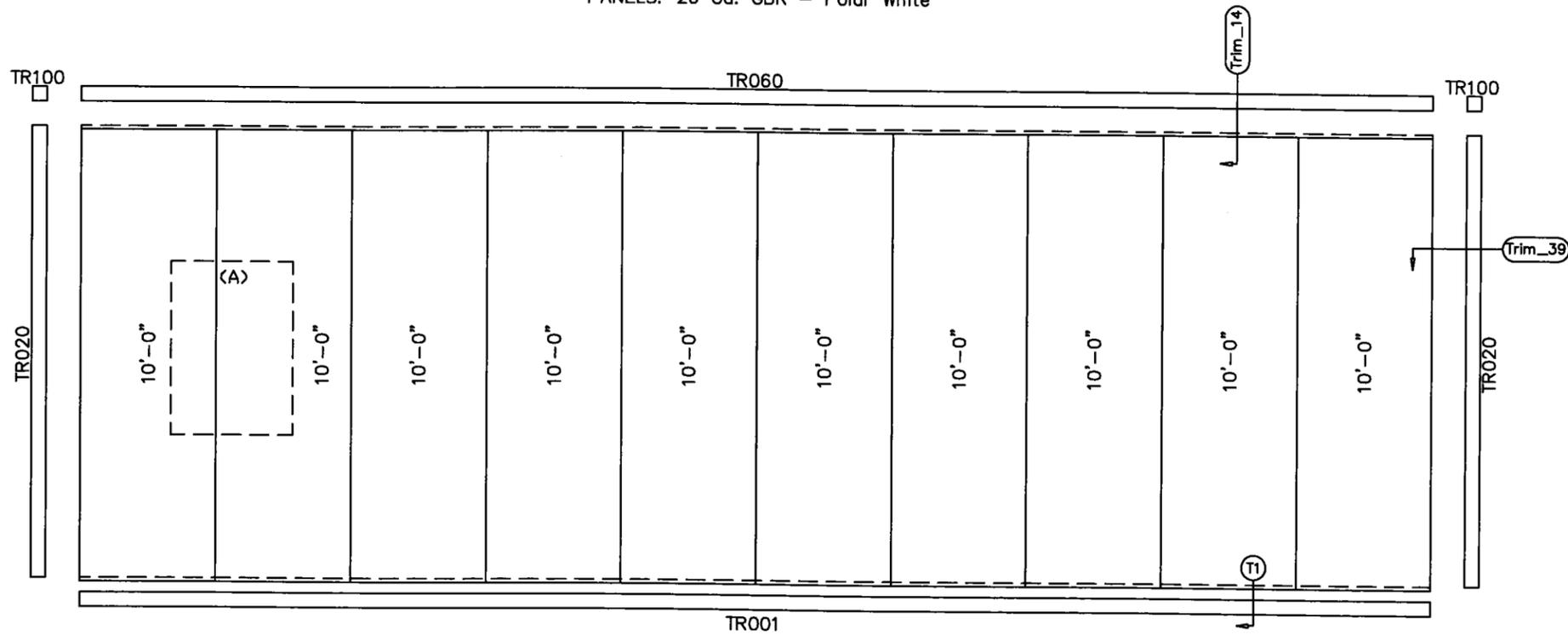
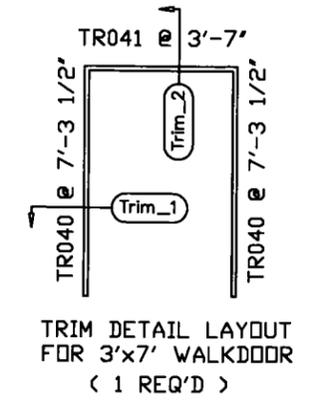
LOW PROFILE RIDGE VENT
 1'-1 1/4"x10'-0" WITH 3 1/2" THROAT
 (2 REQ'D) (FIELD LOCATE AT RIDGE)
 ERECTOR NOTE:
 (50) #14x7/8" S.D. SCREWS,
 (8) OUTSIDE CLOSURES AND 50' OF MASTIC
 PROVIDED FOR EACH VENT.

GENERAL NOTES:
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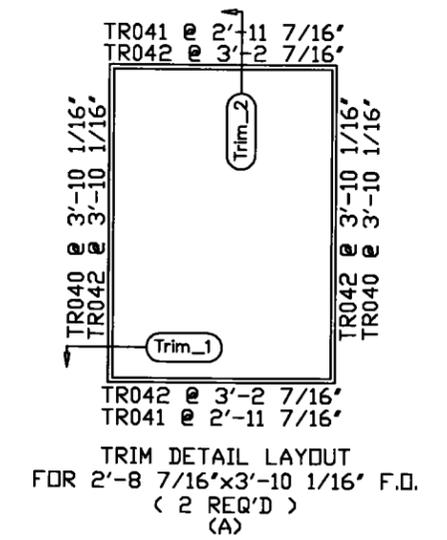
BISON STEEL BUILDINGS, INC.		SEABOARD REMEDIAL ACTION TRUST FUND	
City: MINNEAPOLIS	State: MN	City: GREENSBORO	State: NC
Designer: DAZ	Date: 3/18/13	Drafter: HTS	Date: 3/18/13
Detailer:	Date:	Office:	Job No.:
Checker:	Date:	Office:	16927
ROOF FRAMING & SHEETING			Sht. E6 of 12



SIDEWALL SHEETING & TRIM: FRAME LINE A
 PANELS: 26 Ga. GBR - Polar White

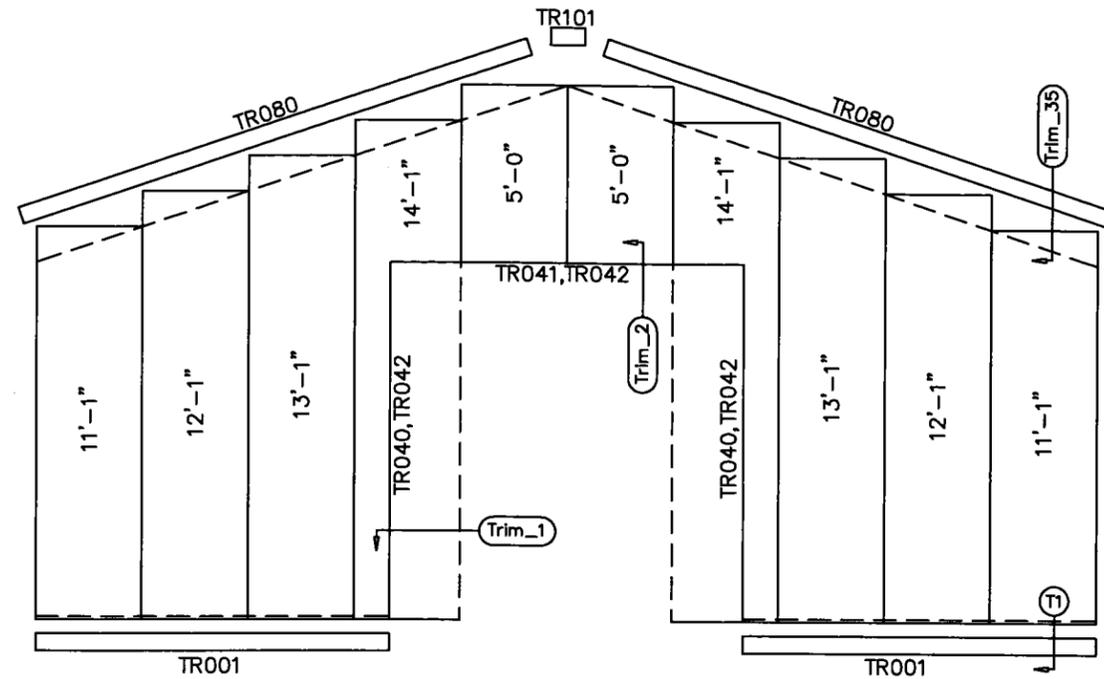


SIDEWALL SHEETING & TRIM: FRAME LINE E
 PANELS: 26 Ga. GBR - Polar White

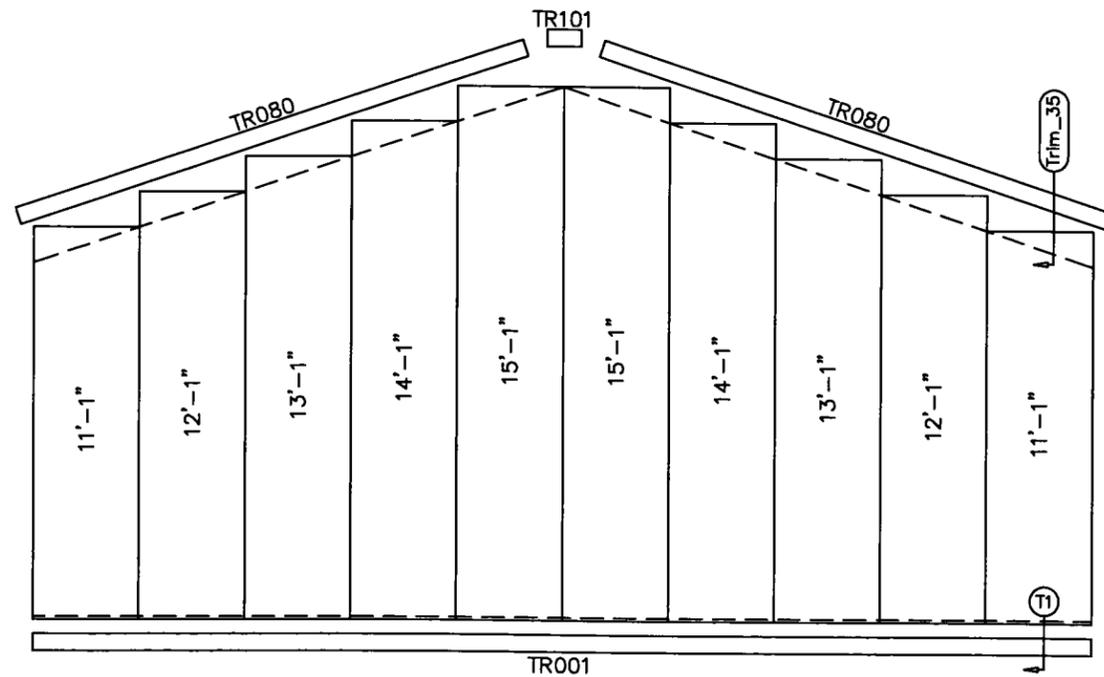


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Designer: DAZ	Date: 3/18/13	Drafter: HTS	Date: 3/18/13
Detailer:	Date:	Office:	Job No.:
Checker:	Date:	Office:	16927
SIDEWALL SHEETING			Sht. E7 of 12



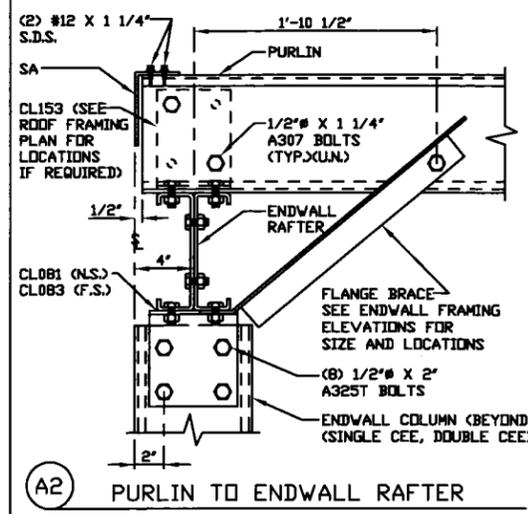
ENDWALL SHEETING & TRIM: FRAME LINE 1
 PANELS: 26 Ga. GBR - Polar White



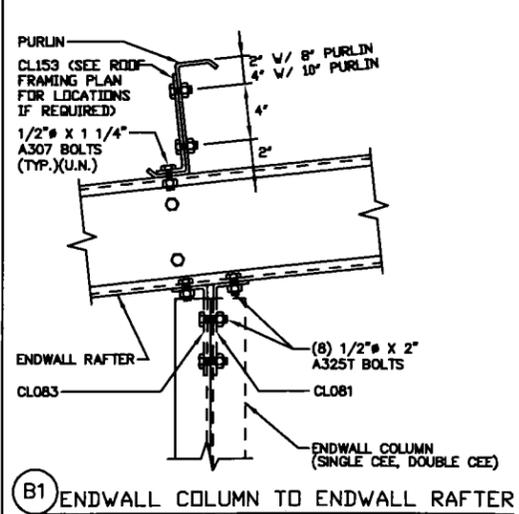
ENDWALL SHEETING & TRIM: FRAME LINE 3
 PANELS: 26 Ga. GBR - Polar White

GENERAL NOTES:
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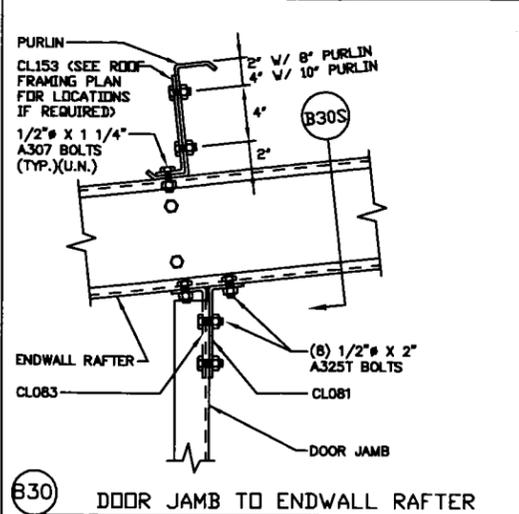
BISON STEEL BUILDINGS, INC.		SEABOARD REMEDIAL ACTION TRUST FUND	
City: MINNEAPOLIS	State: MN	City: GREENSBORO	State: NC
Designer: DAZ	Date: 3/18/13	Drafter: HTS	Date: 3/18/13
Detailer:	Date:	Office:	Job No.:
Checker:	Date:	Office:	16927
ENDWALL SHEETING			Sht. E8 of 12



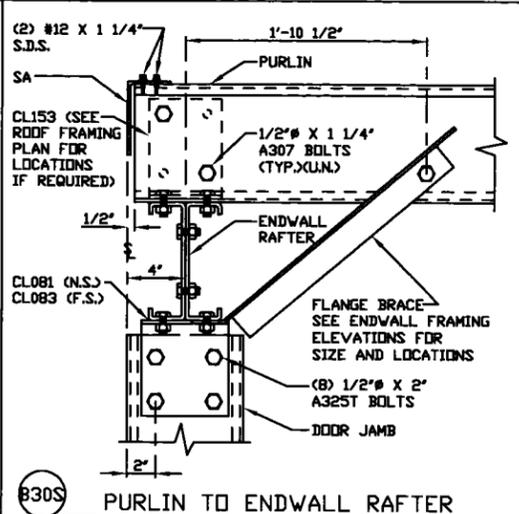
A2 PURLIN TO ENDWALL RAFTER



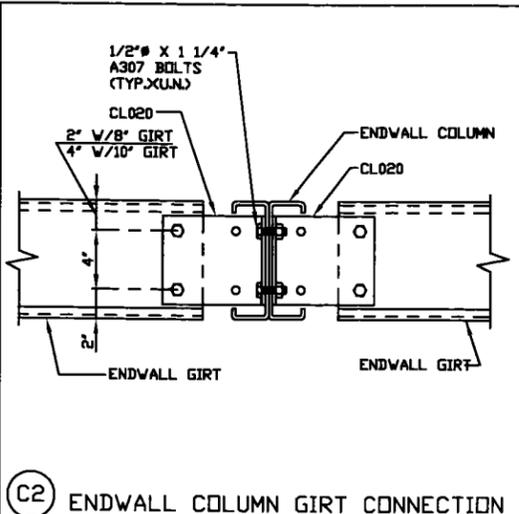
B1 ENDWALL COLUMN TO ENDWALL RAFTER



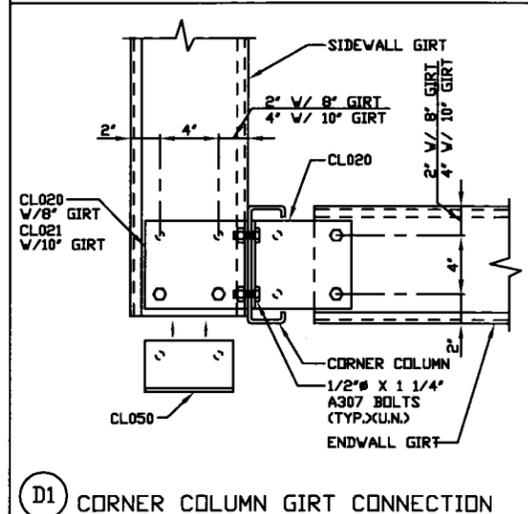
B30 DOOR JAMB TO ENDWALL RAFTER



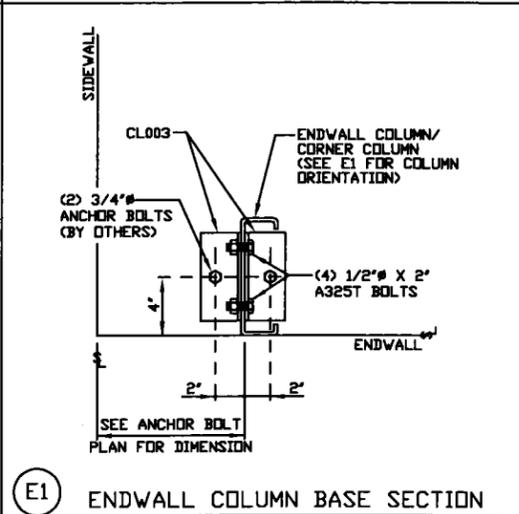
B30S PURLIN TO ENDWALL RAFTER



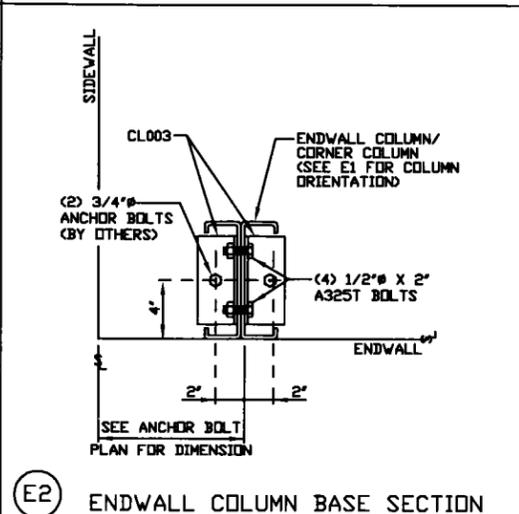
C2 ENDWALL COLUMN GIRT CONNECTION



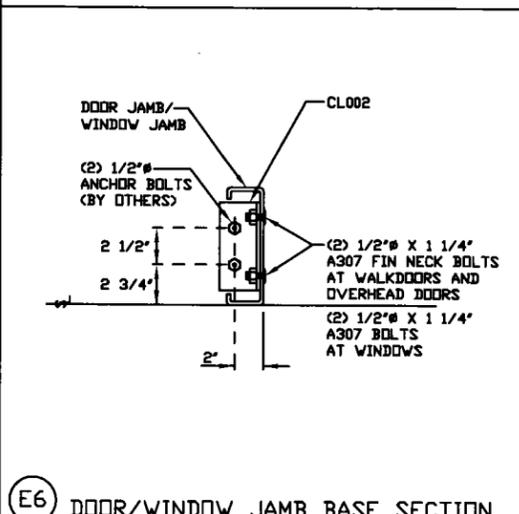
D1 CORNER COLUMN GIRT CONNECTION



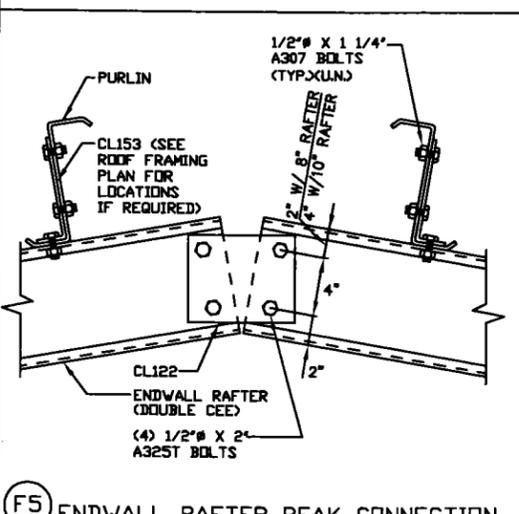
E1 ENDWALL COLUMN BASE SECTION



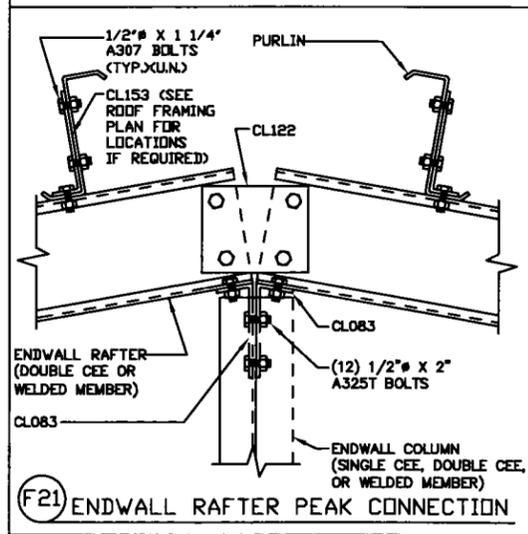
E2 ENDWALL COLUMN BASE SECTION



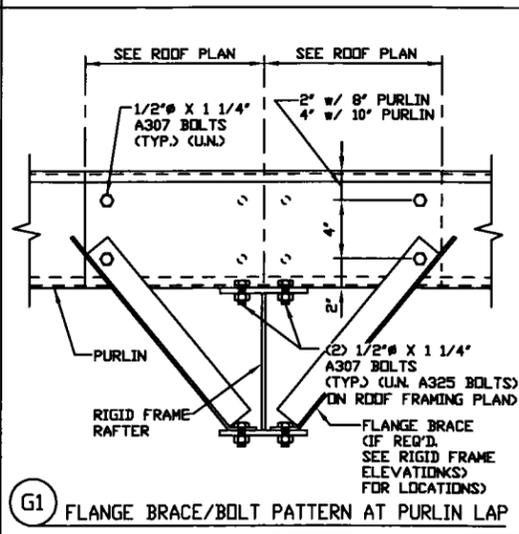
E6 DOOR/WINDOW JAMB BASE SECTION



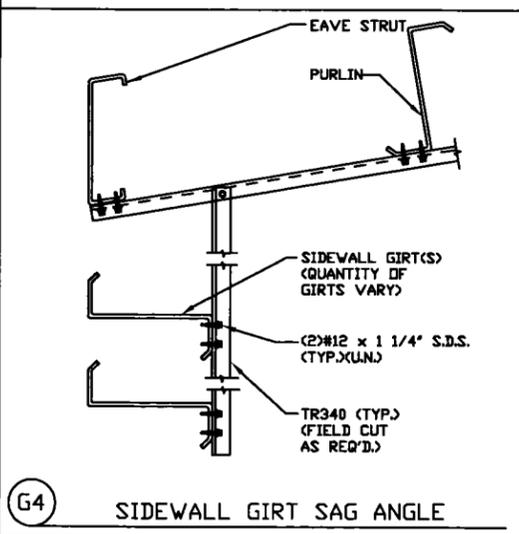
F5 ENDWALL RAFTER PEAK CONNECTION



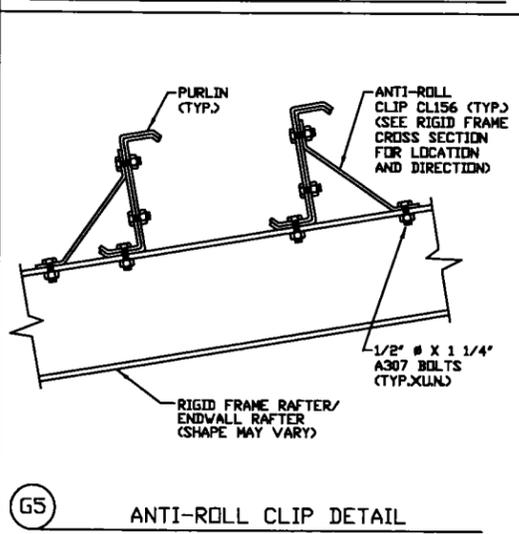
F21 ENDWALL RAFTER PEAK CONNECTION



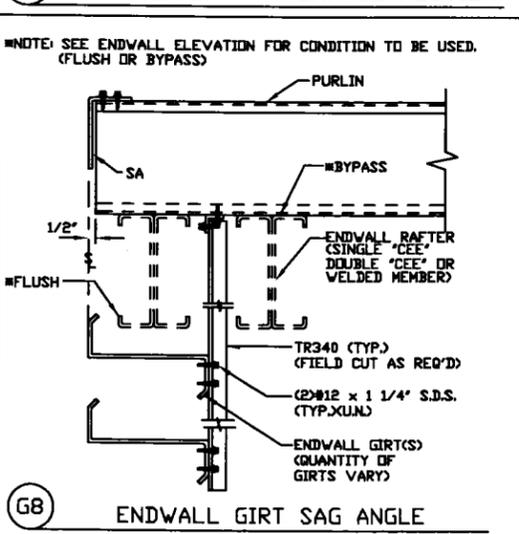
G1 FLANGE BRACE/BOLT PATTERN AT PURLIN LAP



G4 SIDEWALL GIRT SAG ANGLE



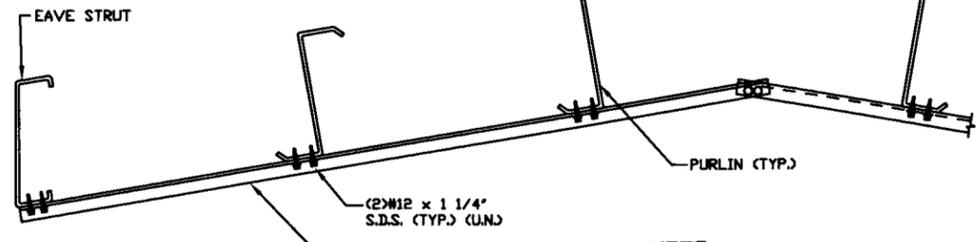
G5 ANTI-ROLL CLIP DETAIL



G8 ENDWALL GIRT SAG ANGLE

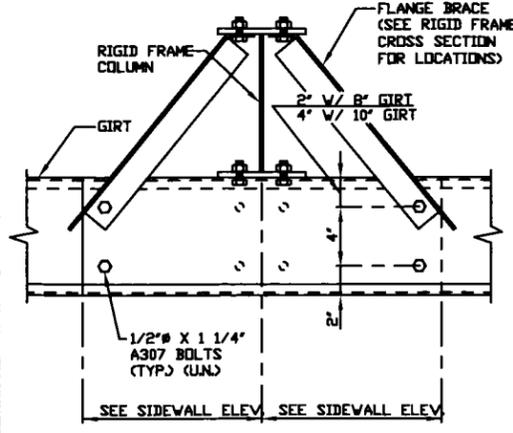
NOTES: 1.) WEB BOLTS IN DOUBLE "C" RAFTERS TO BE AT ENDS, EACH PURLIN, AND MID-POINT BETWEEN PURLINS WITH A MAXIMUM SPACE OF 2'-6".
 2.) WEB BOLTS IN DOUBLE "C" COLUMNS TO BE AT ENDS, EACH GIRT, AND MID-POINT BETWEEN GIRTS WITH A MAXIMUM SPACE OF 3'-8".
 3.) ALL SCREWS ARE WITH WASHERS UNLESS NOTED.

BISON STEEL BUILDINGS, INC.		SEABOARD REMEDIAL ACTION TRUST FUND	
City: MINNEAPOLIS	State: MN	City: GREENSBORO	State: NC
Designer: DAZ	Date: 3/18/13	Drafter: HTS	Date: 3/18/13
Detailer:	Date:	Office:	Job No.:
Checker:	Date:	Office:	16927
DETAIL DRAWINGS			Sht. E9 of 12

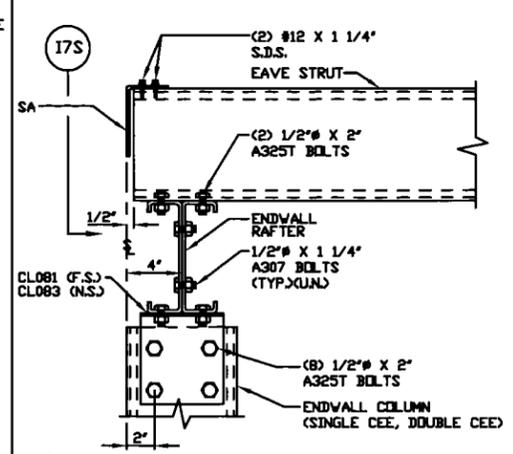


G10 PURLIN SAG ANGLE DETAIL

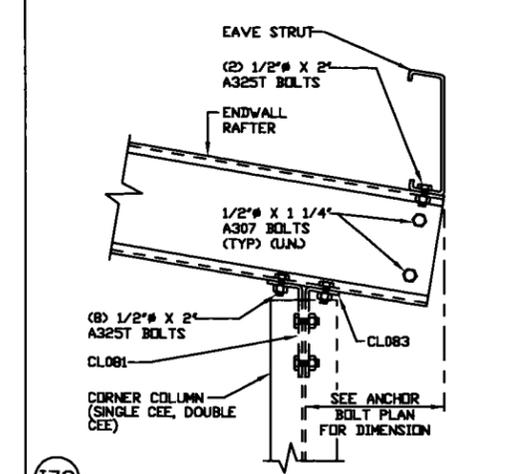
NOTE:
LAPPING MAY BE REQUIRED FOR PROPER INSTALLATION OF TR340. EACH LAP MUST OCCUR AT A PURLIN LOCATION. ANY CUTS WILL BE MADE IN THE FIELD AS THE TR340 IS SUPPLIED IN 20'-0" PIECES.



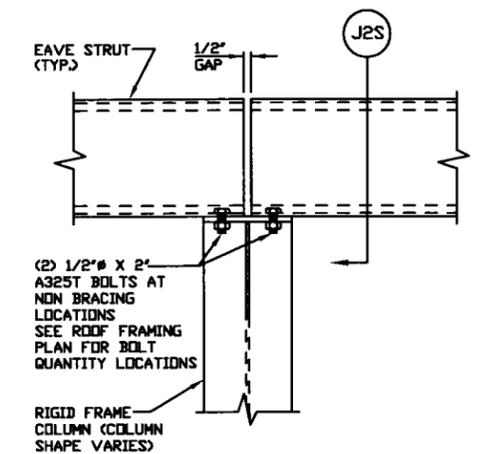
H1 2x2 SIDEWALL GIRT CONNECTION



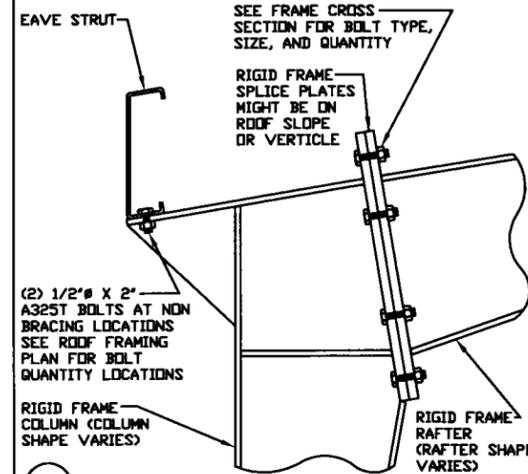
I7 CORNER COLUMN TO ENDWALL RAFTER



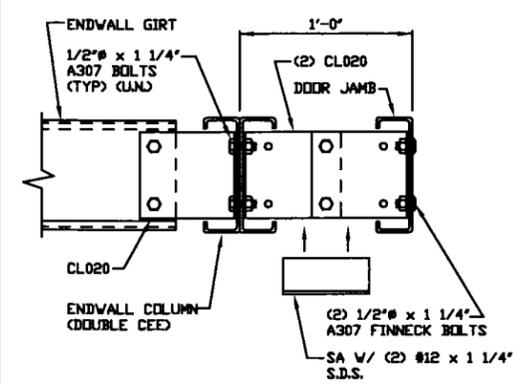
I7S CORNER COLUMN TO ENDWALL RAFTER



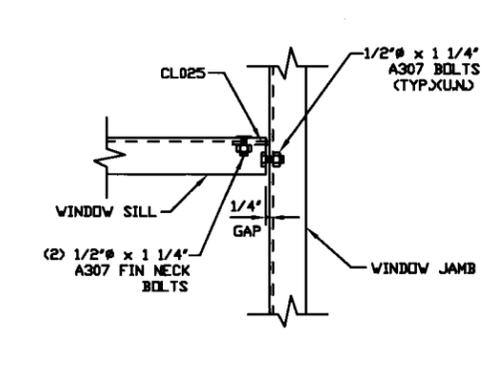
J2 EAVE STRUT TO RIGID FRAME



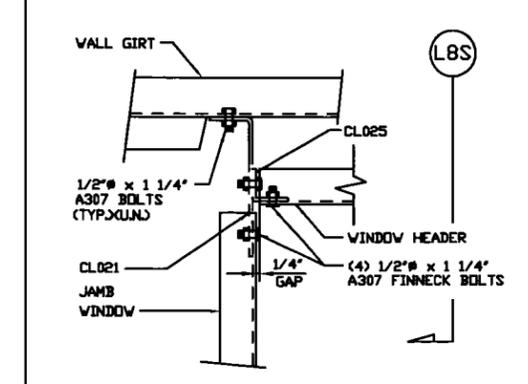
J2S EAVE STRUT TO RIGID FRAME



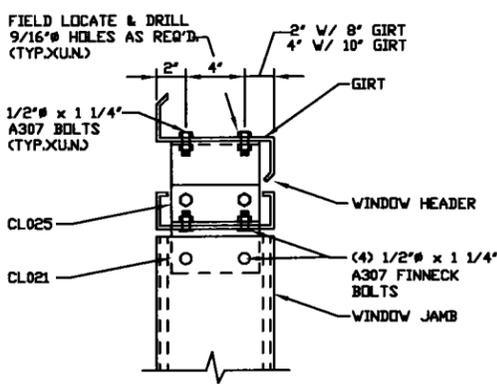
K4 ENDWALL COLUMN GIRT CONNECTION



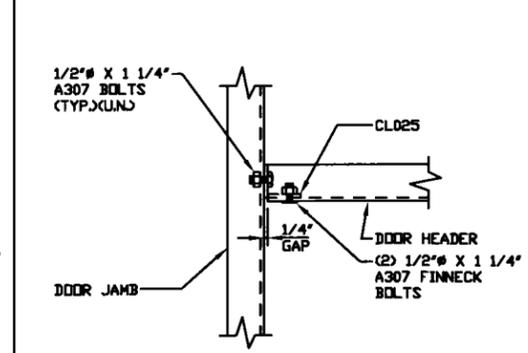
K9 WINDOW SILL TO WINDOW JAMB



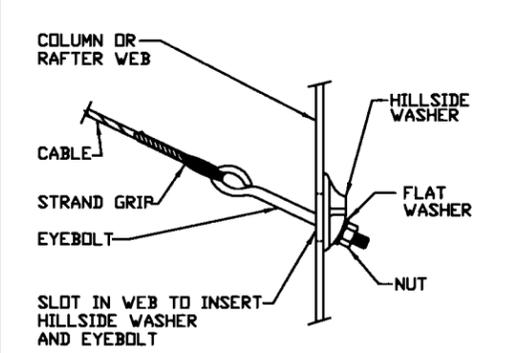
L8 WINDOW JAMB TO WALL GIRT



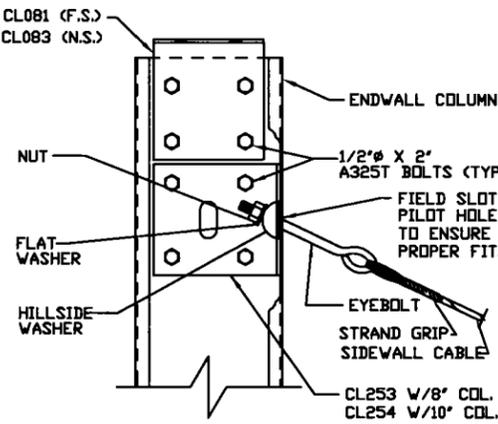
L8S WINDOW JAMB TO WALL GIRT



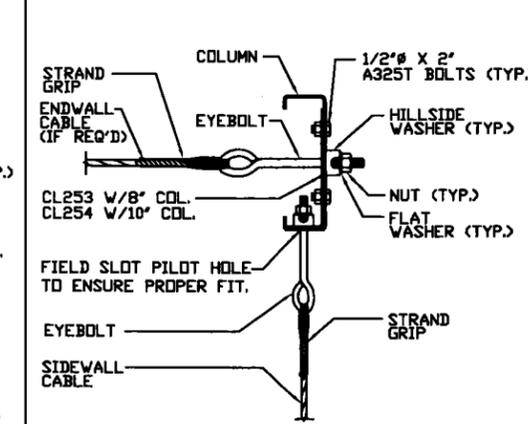
M1 HEADER TO DOOR JAMB



Q2 DIAGONAL CABLE BRACE CONNECTION

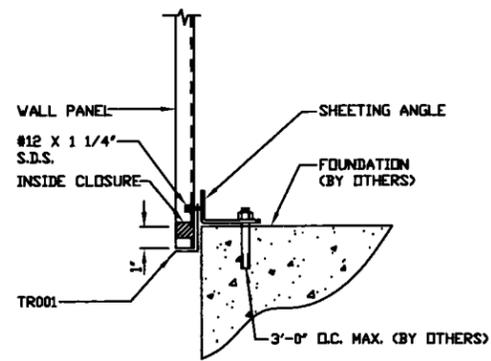


Q8 CABLE TO ENDWALL COLUMN

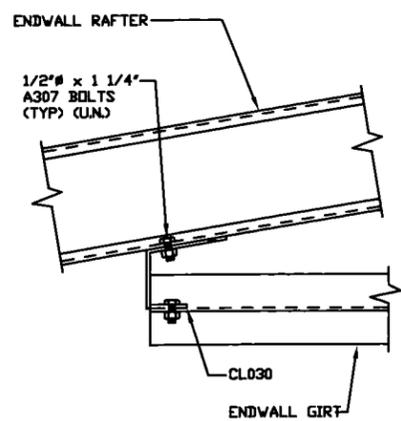


Q9 DIAGONAL CABLE BRACE CONNECTION

BISON STEEL BUILDINGS, INC.		SEABOARD REMEDIAL ACTION TRUST FUND	
City: MINNEAPOLIS	State: MN	City: GREENSBORO	State: NC
Designer: DAZ	Date: 3/18/13	Drafter: HTS	Date: 3/18/13
Detailer:	Date:	Office:	Job No.:
Checker:	Date:	Office:	16927
DETAIL DRAWINGS			Sht. E10 of 12

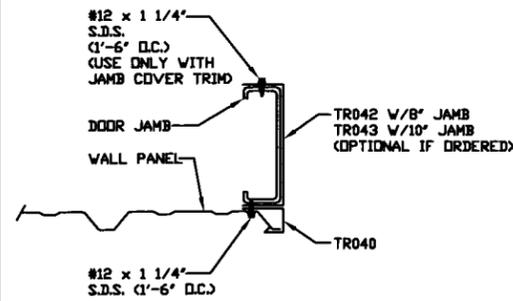


T1 BASE TRIM SECTION

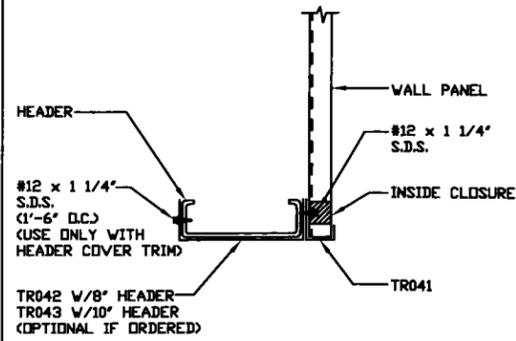


W2 ENDWALL GIRT TO ENDWALL RAFTER

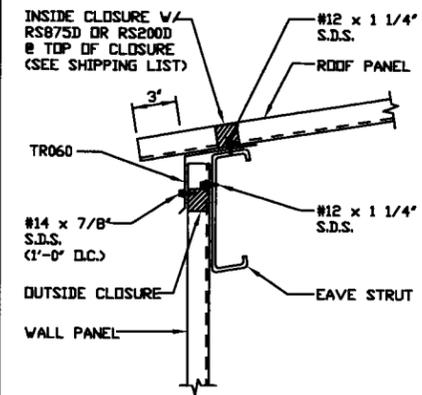
BISON STEEL BUILDINGS, INC.		SEABOARD REMEDIAL ACTION TRUST FUND	
City: MINNEAPOLIS	State: MN	City: GREENSBORO	State: NC
Designer: DAZ	Date: 3/18/13	Drafter: HTS	Date: 3/18/13
Detailer:	Date:	Office:	Job No.:
Checker:	Date:	Office:	16927
DETAIL DRAWINGS			Sht. E11 of 12



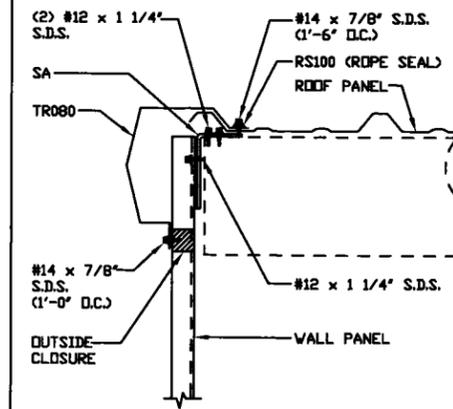
Trim_1 DOOR JAMB TRIM



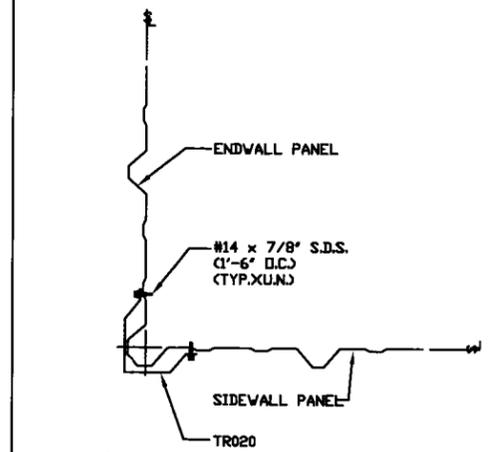
Trim_2 HEADER TRIM



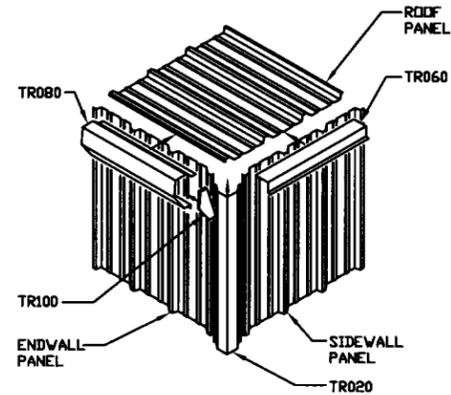
Trim_14 EAVE TRIM SECTION



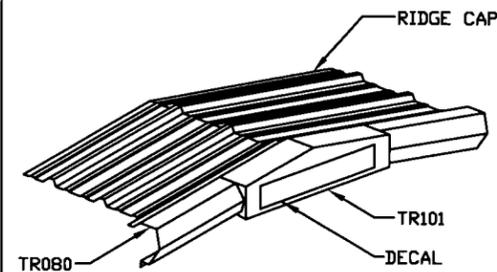
Trim_35 RAKE TRIM SECTION



Trim_39 CORNER TRIM SECTION

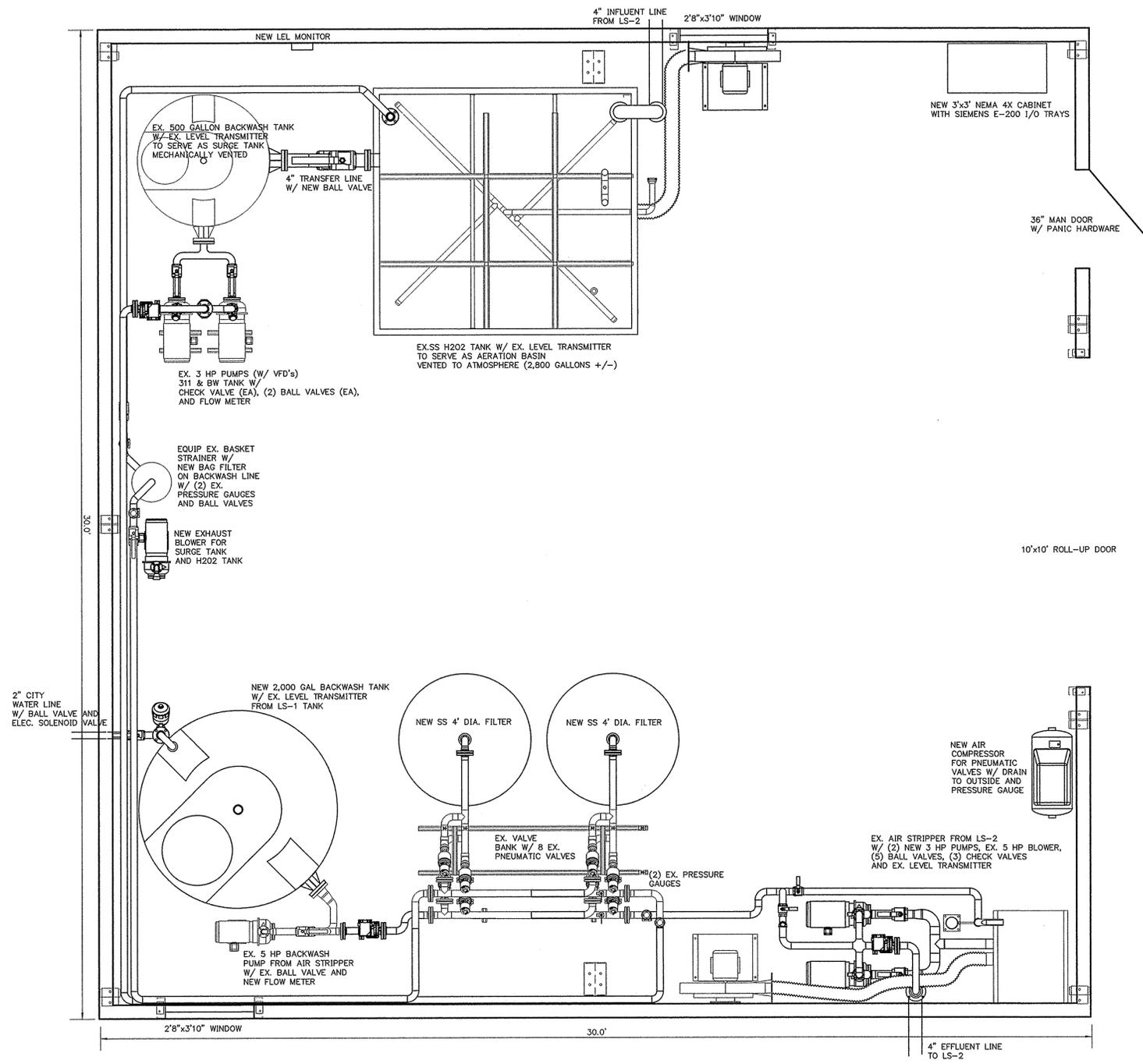


BUILDING CORNER DETAIL



PEAK DETAIL

BISON STEEL BUILDINGS, INC.		SEABOARD REMEDIAL ACTION TRUST FUND	
City: MINNEAPOLIS	State: MN	City: GREENSBORO	State: NC
Designer: DAZ	Date: 3/18/13	Drafter: HTS	Date: 3/18/13
Detailer:	Date:	Office:	Job No.:
Checker:	Date:	Office:	16927
TRIM DRAWINGS			Sht. E12 of 12



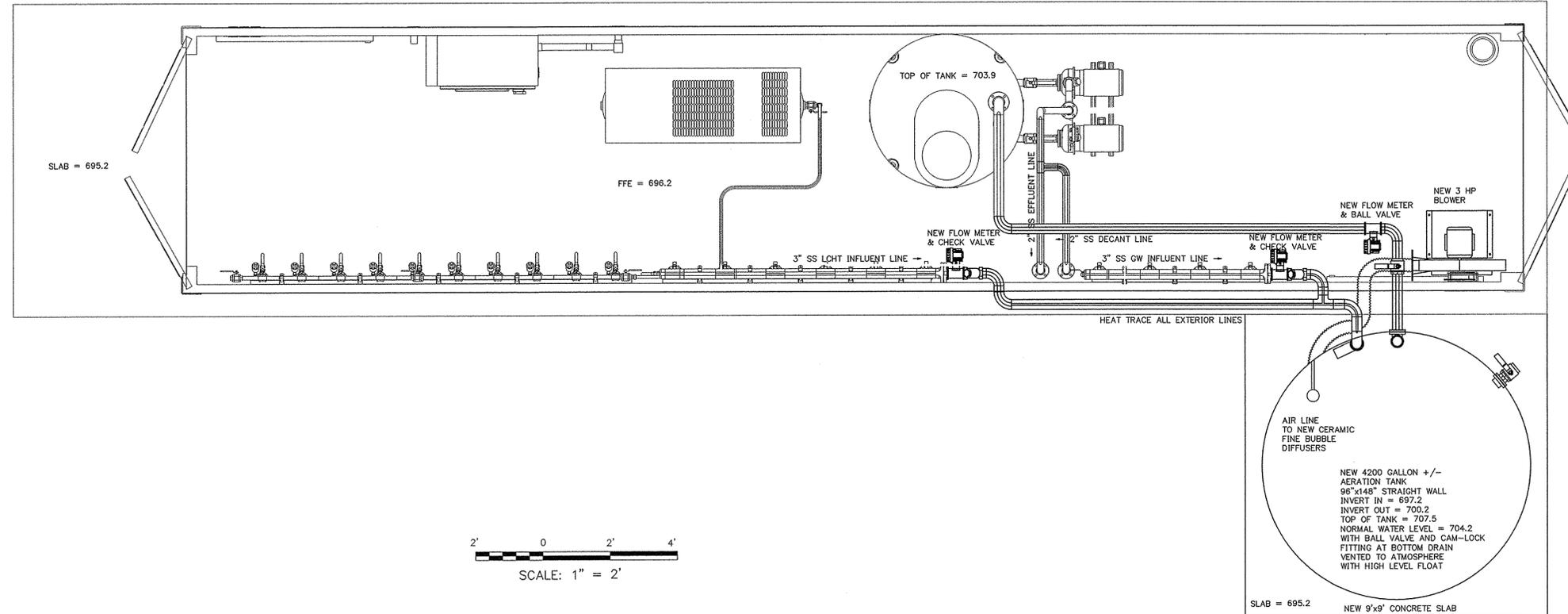
JAMESTOWN ENGINEERING GROUP, INC.
 CONSULTING ENGINEERS
 117 E. MAIN STREET
 P.O. BOX 365
 JAMESTOWN, N.C. 27282
 Telephone (336) 886-5523
 C - 0526



JOB NUMBER	2005165	DATE	FEBRUARY 2013
DESIGNED	T.R.G.	DRAWN	T.R.G.
CHECKED	D.W.P.	BY	
SCALE		DESCRIPTION	

FLOOR PLAN
 SEABOARD GROUP II &
 THE CITY OF HIGH POINT
 FILTER BUILDING
 CITY OF HIGH POINT
 GUILFORD COUNTY - NORTH CAROLINA

SHEET NO.
 C-2
 LS-2-REVISED.DWG
 02/28/13 3:15 PM



2' 0 2' 4'
SCALE: 1" = 2'



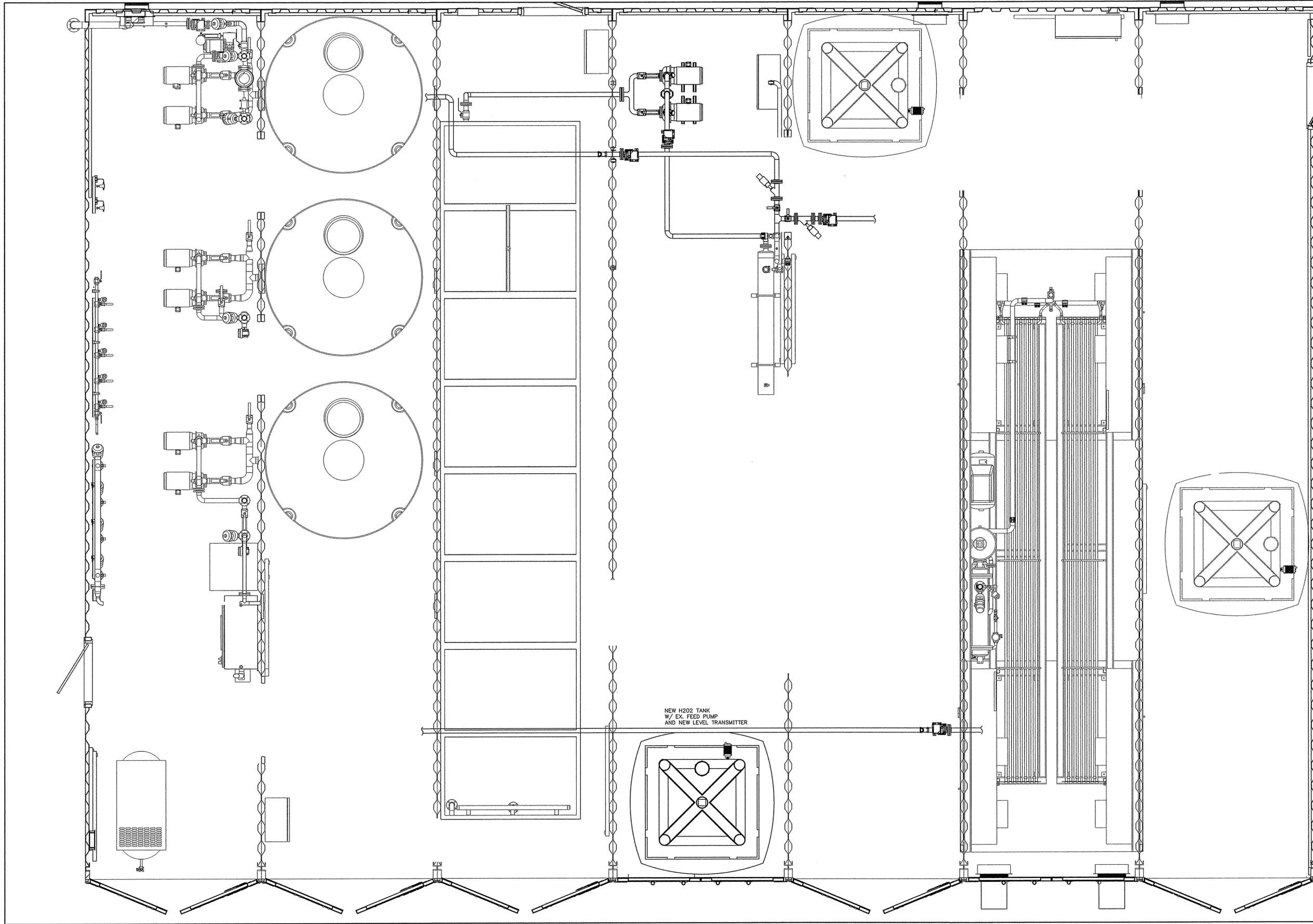
JAMESTOWN ENGINEERING GROUP, INC.
CONSULTING ENGINEERS
117 E. MAIN STREET
P.O. BOX 365
JAMESTOWN, N.C. 27651
Telephone: 888-5523
Fax: 888-0626



REV.	DATE	DESCRIPTION	BY	SCALE
DESIGNED	FEBRUARY 2013	I.R.G.		
DRAWN		T.R.G.		
CHECKED		D.W.P.		

SITE PLAN
SLABGROUP II &
THE CITY OF HIGH POINT
LS-1 REVISIONS
CITY OF HIGH POINT
GUILFORD COUNTY - NORTH CAROLINA

SHEET NO.
C-3
LS-1 REVISIONS DATE
02/27/13 13:01



NEW H2O2 TANK
W/ EX. FEED PUMP
AND NEW LEVEL TRANSMITTER

SHEET NO.
C-4
LS-2-REVISED.DWG
02/26/13 3:18 PM

SITE PLAN
**SEABOARD GROUP II &
THE CITY OF HIGH POINT**
LS-2 REVISIONS
CITY OF HIGH POINT
GUILFORD COUNTY - NORTH CAROLINA

REV.	DATE	DESCRIPTION	BY

JOB NUMBER	2005165
DATE	FEBRUARY 2013
DESIGNED	T.R.G.
DRAWN	T.R.G.
CHECKED	D.W.P.
SCALE	

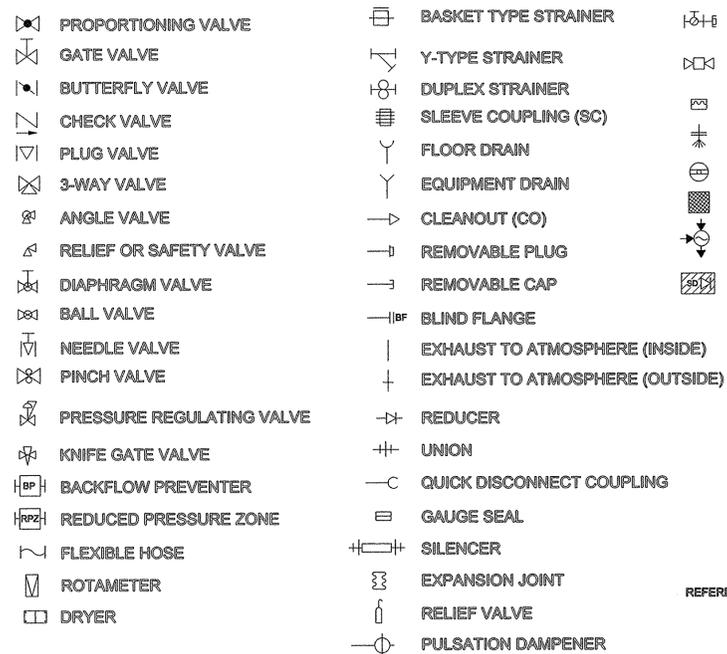


JAMESTOWN ENGINEERING GROUP, INC.
CONSULTING ENGINEERS
117 E. MAIN STREET
JAMESTOWN, N.C. 27282
Telephone (336) 886-5523
C - 0626



6/28/13

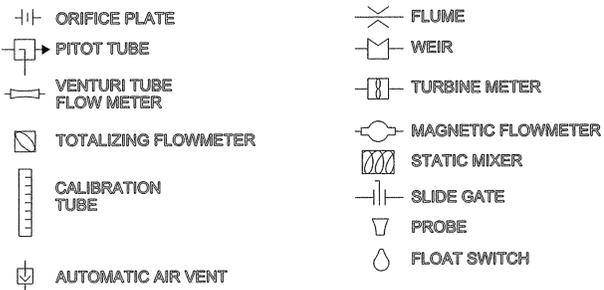
VALVE AND PIPING SYMBOLS



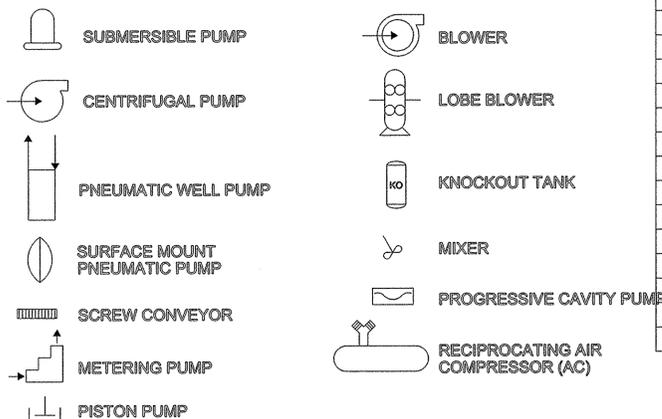
VALVE OPERATOR SYMBOLS



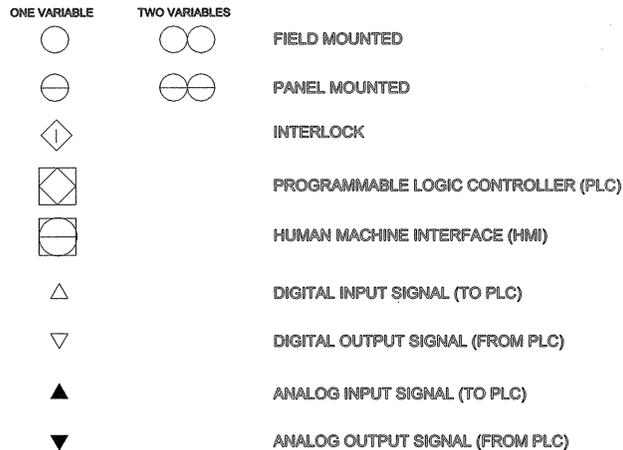
PRIMARY ELEMENT SYMBOLS - FLOW



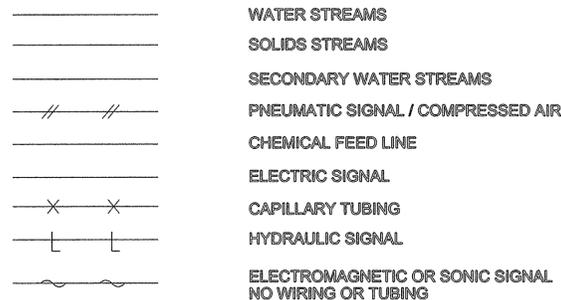
EQUIPMENT SYMBOLS



GENERAL INSTRUMENT SYMBOLS



LINE SYMBOLS



REFERENCE MARKER



PROCESS LINE ABBREVIATIONS

AIR	AIR, ATMOSPHERIC PRESSURE
BW	BACKWASH
CA	COMPRESSED AIR
CCA	CHLORINE CONTAMINATED AIR
CSW	CONTAMINATED GROUNDWATER
D	DRAIN
EFF	EFFLUENT
EXH	EXHAUST
FLT	FILTRATE
FTW	FILTER-TO-WASTE
NPW	NON-POTABLE WATER
OZE	OZONE GAS
P	PRODUCT
PW	POTABLE WATER
RW	RAW WATER
S	SANITARY
SL	SLUDGE
SN	SUPERNATANT
SP	SAMPLE PORT
SS	STORM SEWER
TF	TOTAL FLUIDS
TW	TREATED WATER
V	VENT
VAP	VAPOR

PIPING MATERIAL IDENTIFICATION

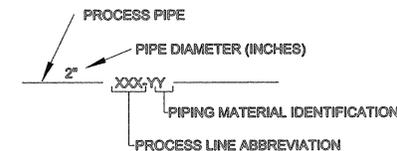
CPVC	CHLORINATED POLYVINYL CHLORIDE
CSP	CARBON STEEL PIPE
COP	COPPER
CMP	CORRUGATED METAL PIPE
CIP	CAST IRON PIPE
DIP	DUCTILE IRON PIPE
FRP	FIBERGLASS REINFORCED PIPE
GSP	GALVANIZED STEEL PIPE
HDPE	HIGH DENSITY POLYETHYLENE PIPE
PE	POLYETHYLENE PIPE
PP	POLYPROPYLENE PIPE
PVC	POLYVINYL CHLORIDE PIPE
RCP	REINFORCED CONCRETE PIPE
RUB	RUBBER
SS	STAINLESS STEEL PIPE
VCP	VITRIFIED CLAY PIPE

EQUIPMENT NOTATION ABBREVIATIONS

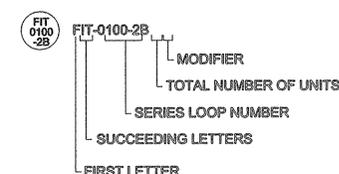
AC	AIR COMPRESSOR	L	LAUNDER
AN	ANNUBAR	MX	MIXER
ARV	AIR RELIEF VALVE	OP	ORIFICE PLATE
B	BLOWER	P	PUMP
BFP	BELT FILTER PRESS	PB	POLYMER AIRLOCK
BP	BOOSTER PUMP	PCV	PRESSURE CONTROL VALVE
BPD	BACKFLOW PREVENTION DEVICE	PD	PULSATION DAMPENERS
C	CATALYST	PW	PRESSURE WASHER
CA	COLLECTOR ARM	FWC	FRE WETTING COIL
CC	CALIBRATION COLUMN (LG)	RA	ROTARY AIRLOCK
CL	CHLORINATOR	RM	ROTOMETER
CV	CHECK VALVE	S	STORAGE
CY	CYCLONE	SB	STORAGE BIN
D	DIFFUSERS	SC	SCALE
E	EDUCTOR	SIL	SILENCER
FC	FILTER CELL	SM	STATIC MIXER
FM	FLOW METER	SP	SAMPLE PUMP
FV	FLOW VALVE	SV	SOLENOID VALVE
GC	GRIT CLASSIFIER	SW	STILLING WELL
GS	GAS SENSOR	T	TANK
GT	GRAVITY THICKENER	V	VIBRATOR
H	HYDROCYCLONE	VR	AUTOMATIC SWITCHOVER VACUUM REGULATOR
HP	HOPPER	WP	W/ TRAP & FILTER
HV	HAND VALVE	WW	ADJUSTABLE WEIR PLATE
IN	INJECTOR		WETWELL

INSTRUMENT IDENTIFICATION TABLE					
FIRST LETTER			SUCCEEDING LETTERS		
	MEASURED OR INITIATING VARIABLE	MODIFIER	READOUT OR PASSIVE FUNCTION	OUTPUT FUNCTION	MODIFIER
A	ANALYSIS		ALARM		
B	BURNER, COMBUSTION				
C	CONDUCTIVITY			CONTROL	CLOSED
D	DENSITY (SP. GR.)	DIFFERENTIAL			
E	VOLTAGE		SENSOR (PRIMARY ELEMENT)		
F	FLOW RATE	RATIO (FRACTION)			
G	GAGING (DIMENSIONAL)		GLASS, VIEWING DEVICE		
H	HAND				HIGH
I	CURRENT		INDICATE		
J	POWER	SCAN			
K	TIME, TIME SCHEDULE	TIME RATE CHANGE		CONTROL STATION	
L	LEVEL		LIGHT		LOW
M	MOTOR	MOMENTARY			MIDDLE, INTERMEDIATE
N	TORQUE		ISOLATE	ISOLATOR	
O	OPERATION		ORIFICE, RESTRICTION		OPEN
P	PRESSURE, VACUUM		POINT (TEST) CONNECTION		
Q	QUANTITY	INTEGRATE, TOTALIZE			
R	RADIATION		RECORD		
S	SPEED OR FREQUENCY	SAFETY		SWITCH	
T	TEMPERATURE			TRANSMIT	
U	MULTIVARIABLE		MULTIFUNCTION	MULTIFUNCTION	MULTIFUNCTION
V	VIBRATION, MECHANICAL ANALYSIS			VALVE OR DAMPER, LOUVER	
W	WEIGHT OR FORCE		WELL		
X	UNCLASSIFIED	X-AXIS			
Y	EVENT, STATE OR PRESENCE	Y-AXIS		RELAY OR COMPUTE, CONVERT	
Z	POSITION, DIMENSION	Z-AXIS		DRIVE, ACTUATOR	

PROCESS PIPING IDENTIFICATION



INSTRUMENT IDENTIFICATION



FUNCTION ABBREVIATIONS

A	ANALOG	LEL	LOWER EXPLOSIVE LIMIT
AIT	ANALOG INDICATING TRANSMITTER	L	LENGTH
ALT	ALTERNATE	LCP	LOCAL CONTROL PANEL
BFC	BALLASTED FLOCCULATION / CLARIFICATION	LOS	LOCK OUT SERVICE
CL ₂	CHLORINE RESIDUAL	L/R	LOCAL-REMOTE
C	CONTROL STATION	NO	NORMALLY OPEN
D	DIGITAL	NC	NORMALLY CLOSED
dP	DIFFERENTIAL PRESSURE	O ₃	OZONE GAS
DO	DISSOLVED OXYGEN	OAC	OPEN-AUTO-CLOSE
f	INTERNAL INDICATOR	OC	OPEN-CLOSE
FC	FAIL CLOSED	OD	ON-OFF...MAINTAINED
FI	FAIL INDETERMINATE	ORP	OXIDATION REDUCTION POTENTIAL
FL	FAIL LOCKED	OSC	OPEN-STOP-CLOSE...MOMENTARY
FO	FAIL OPEN	SEQ	SEQUENCE OPERATION
HMI	HUMAN MACHINE INTERFACE	SP	SET POINT
HOA	HAND-OFF-AUTOMATIC	S/S	START-STOP...MOMENTARY
HS	HAND SWITCH	TOAE	TIME-TO-OPEN AFTER ENERGIZED
IAS	INTERNAL AIR SUPPLY	TURB	TURBIDITY
I/I	CURRENT-TO-CURRENT	UCP	UNIT CONTROL PANEL
I/P	CURRENT-TO-PNEUMATIC	VGAC	VAPOR-PHASE GRANULAR ACTIVATED CARBON
		VM	VOLTAGE MONITOR
		>	HIGH SELECT
		<	LOW SELECT

NOT FOR CONSTRUCTION - FOR BIDDING PURPOSES ONLY

CHEMTECH ENGINEERING, INC.
11254 SUNSET BAY NORTHPORT, ALABAMA 35475
Telephone: (205) 339-0689 Fax: (205) 339-4487

NO.	DATE	APPR.	REVISION	NO.	DATE	APPR.	REVISION
0	12-14-09	S. Lucas	FOR CLIENT REVIEW				
1	5-18-10	S. Lucas	FOR BID PACKAGE SUBMITTAL				
2	11-10-10	S. Lucas	FOR PRE-CONSTRUCTION REVIEW				
3	6-20-12		PER INSTALLATION				
4	6-28-13		PER REQUESTED MODIFICATIONS				

**REMEDIATION SYSTEM DESIGN DRAWINGS
FORMER SEABOARD CHEMICAL FACILITY/
RIVERDALE DRIVE LANDFILL SITE**

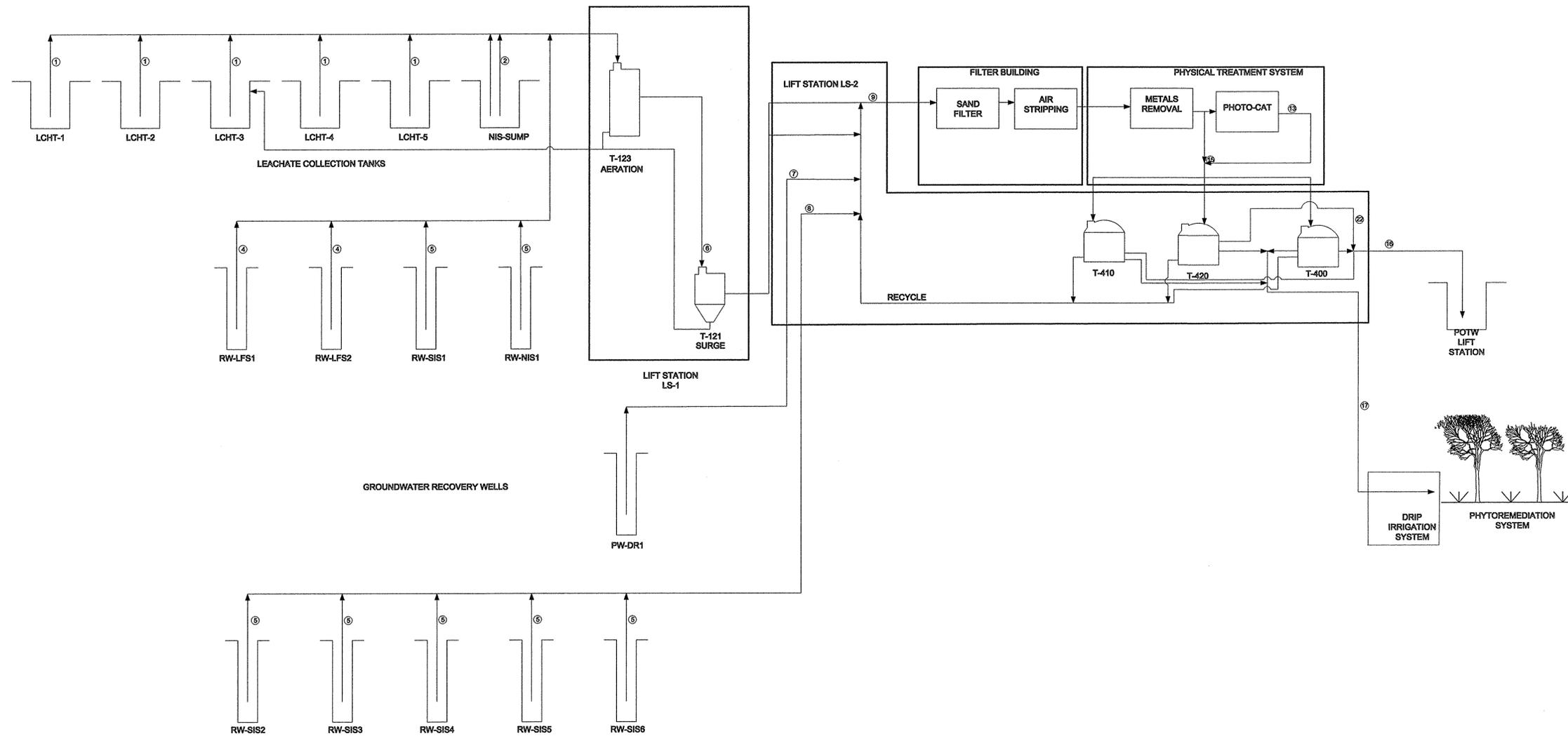
SEABOARD GROUP II JAMESTOWN, NC

DRAWN BY	M. BROWN	PROJECT ENGINEER	R. GLOVER
DESIGN ENGINEER	S. LUCAS	PROJECT MANAGER	J. LARUE

**MECHANICAL TREATMENT
PROCESS AND INSTRUMENTATION DIAGRAM**

SCALE	NTS	DATE	JUNE 28, 2013
PROJECT NO.	05-165 SEABOARD	AutoCAD 2010	PROCESS-FLOW-DIAGRAM.DWG

DRAWING NO. 1-1
REV. NO. 4
SHEET 1 OF 8



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0	12-14-09	S. Lucas	FOR CLIENT REVIEW				
1	5-18-10	S. Lucas	FOR BID PACKAGE SUBMITTAL				
2	11-10-10	S. Lucas	FOR PRE-CONSTRUCTION REVIEW				
3	6-20-12		PER INSTALLATION				
4	6-28-13		PER REQUESTED MODIFICATIONS				

**REMEDATION SYSTEM DESIGN DRAWINGS
 FORMER SEABOARD CHEMICAL FACILITY/
 RIVERDALE DRIVE LANDFILL SITE**

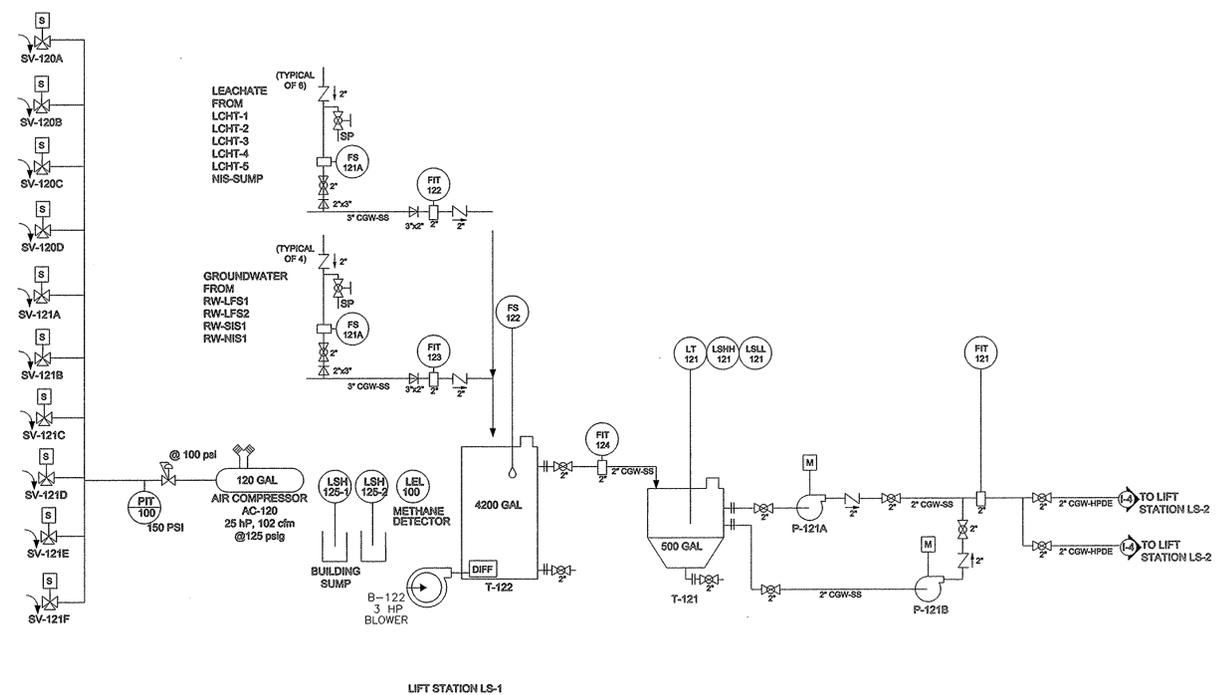
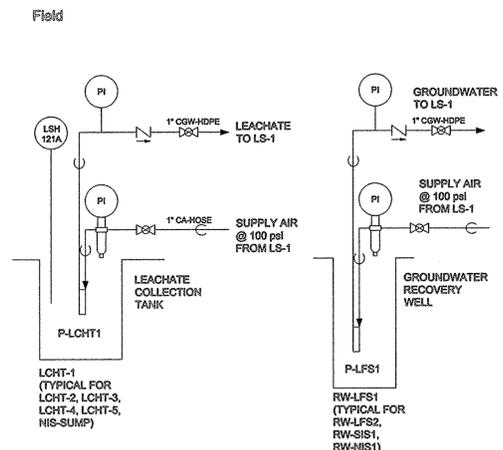
SEABOARD GROUP II JAMESTOWN, NC

DRAWN BY M. BROWN	PROJECT ENGINEER R. GLOVER
DESIGN ENGINEER S. LUCAS	PROJECT MANAGER J. LARUE

**MECHANICAL TREATMENT
 PROCESS AND INSTRUMENTATION DIAGRAM**

SCALE NTS	DATE JUNE 28, 2013
PROJECT NO. 05-165 SEABOARD	AutoCAD 2010 PROCESS-FLOW-DIAGRAM.DWG

DRAWING NO. I-2	REV. NO. 4
SHEET 2	OF 8



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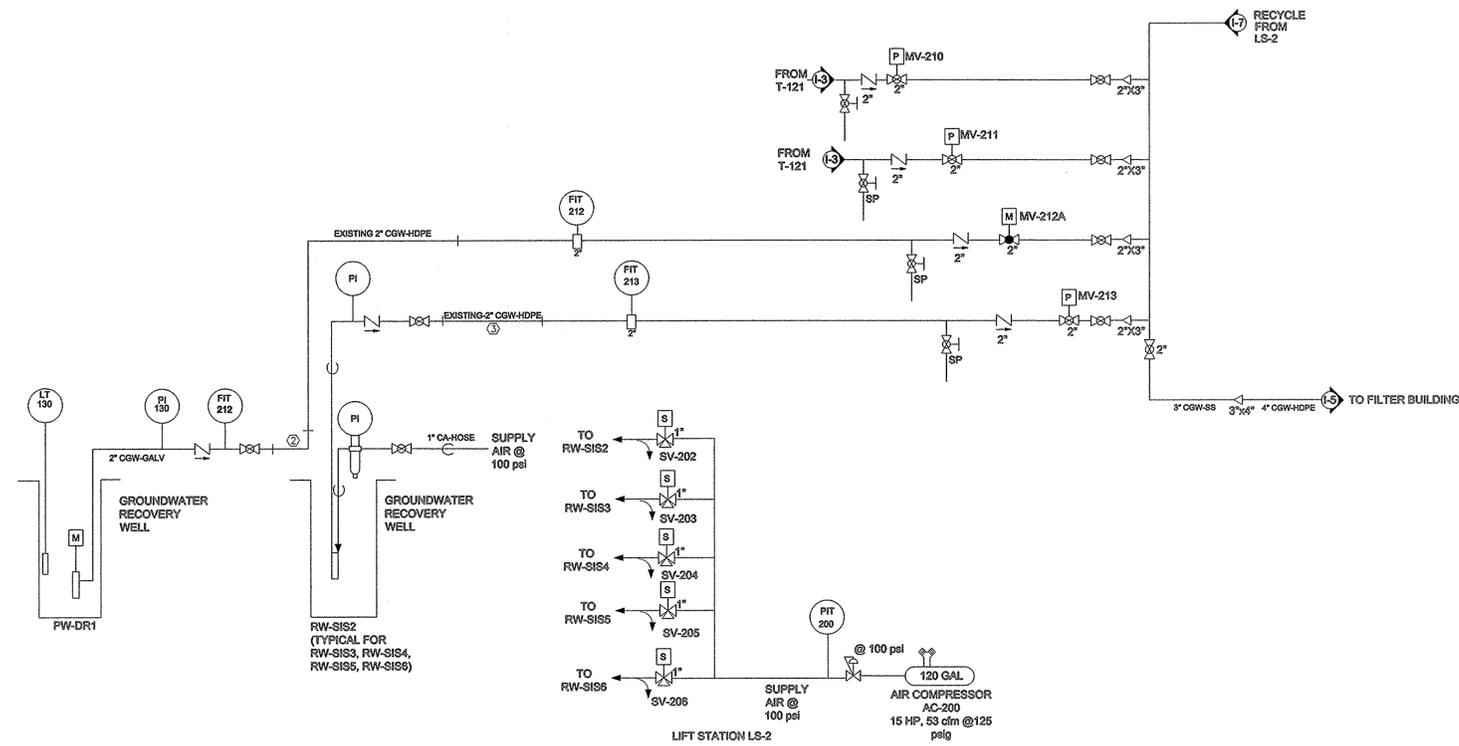
CHEMTECH ENGINEERING, INC.
11254 SUNSET BAY NORTHPORT, ALABAMA 35475
Telephone: (205) 339-0689 Fax: (205) 339-4487

NO.	DATE	APPR.	REVISION	NO.	DATE	APPR.	REVISION
0	12-14-09	S. Lucas	FOR CLIENT REVIEW				
1	5-18-10	S. Lucas	FOR BID PACKAGE SUBMITTAL				
2	11-10-10	S. Lucas	FOR PRE-CONSTRUCTION REVIEW				
3	6-20-12		PER INSTALLATION				
4	6-28-13		PER REQUESTED MODIFICATIONS				

**REMEDATION SYSTEM DESIGN DRAWINGS
FORMER SEABOARD CHEMICAL FACILITY/
RIVERDALE DRIVE LANDFILL SITE**
SEABOARD GROUP II JAMESTOWN, NC

DRAWN BY **M. BROWN** PROJECT ENGINEER **R. GLOVER**
DESIGN ENGINEER **S. LUCAS** PROJECT MANAGER **J. LARUE**

MECHANICAL TREATMENT PROCESS AND INSTRUMENTATION DIAGRAM		DRAWING NO. 1-3
SCALE NTS	DATE JUNE 28, 2013	REV. NO. 4
PROJECT NO. 05-165 SEABOARD	AutoCAD 2010 PROCESS-FLOW-DIAGRAM.DWG	SHEET 3 OF 8



NOT FOR CONSTRUCTION - FOR BIDDING PURPOSES ONLY

CHEMTECH ENGINEERING, INC.
11254 SUNSET BAY NORTHPORT, ALABAMA 35475
Telephone: (205) 339-0689 Fax: (205) 339-4487

NO.	DATE	APPR.	REVISION	NO.	DATE	APPR.	REVISION
0	12-14-09	S. Lucas	FOR CLIENT REVIEW				
1	5-18-10	S. Lucas	FOR BID PACKAGE SUBMITTAL				
2	11-10-10	S. Lucas	FOR PRE-CONSTRUCTION REVIEW				
3	6-20-12		PER INSTALLATION				
4	6-28-13		PER REQUESTED MODIFICATIONS				

**REMEDATION SYSTEM DESIGN DRAWINGS
FORMER SEABOARD CHEMICAL FACILITY/
RIVERDALE DRIVE LANDFILL SITE**

SEABOARD GROUP II JAMESTOWN, NC

DRAWN BY M. BROWN	PROJECT ENGINEER R. GLOVER
DESIGN ENGINEER S. LUCAS	PROJECT MANAGER J. LARUE

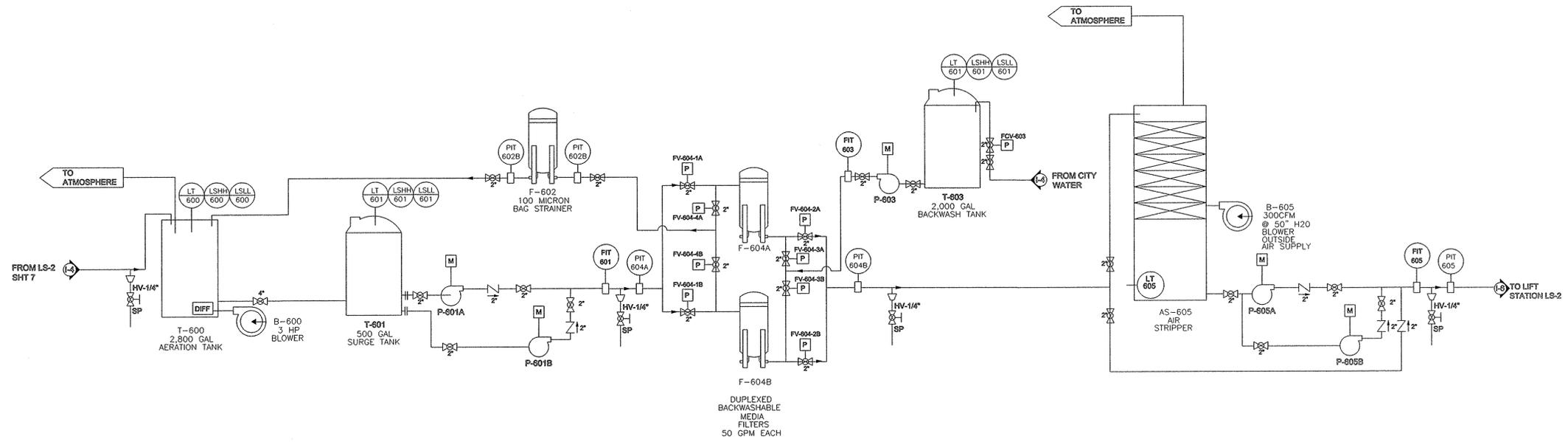
**MECHANICAL TREATMENT
PROCESS AND INSTRUMENTATION DIAGRAM**

SCALE NTS	DATE JUNE 28, 2013
PROJECT NO. 05-165 SEABOARD	AutoCAD 2010 PROCESS-FLOW-DIAGRAM.DWG

DRAWING NO.
I-4

REV. NO.
4

SHEET **4** OF **8**



NOT FOR CONSTRUCTION - FOR BIDDING PURPOSES ONLY

CHEMTECH ENGINEERING, INC.
11254 SUNSET BAY NORTHPORT, ALABAMA 35475
Telephone: (205) 339-0689 Fax: (205) 339-4487

NO.	DATE	APPR.	REVISION	NO.	DATE	APPR.	REVISION
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1	5-18-10	S. Lucas	FOR BID PACKAGE SUBMITTAL				
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3	8-20-12		PER INSTALLATION				
4	6-28-13		PER REQUESTED MODIFICATIONS				

**REMEDATION SYSTEM DESIGN DRAWINGS
FORMER SEABOARD CHEMICAL FACILITY/
RIVERDALE DRIVE LANDFILL SITE**

SEABOARD GROUP II JAMESTOWN, NC

DRAWN BY M. BROWN	PROJECT ENGINEER R. GLOVER
DESIGN ENGINEER S. LUCAS	PROJECT MANAGER J. LARUE

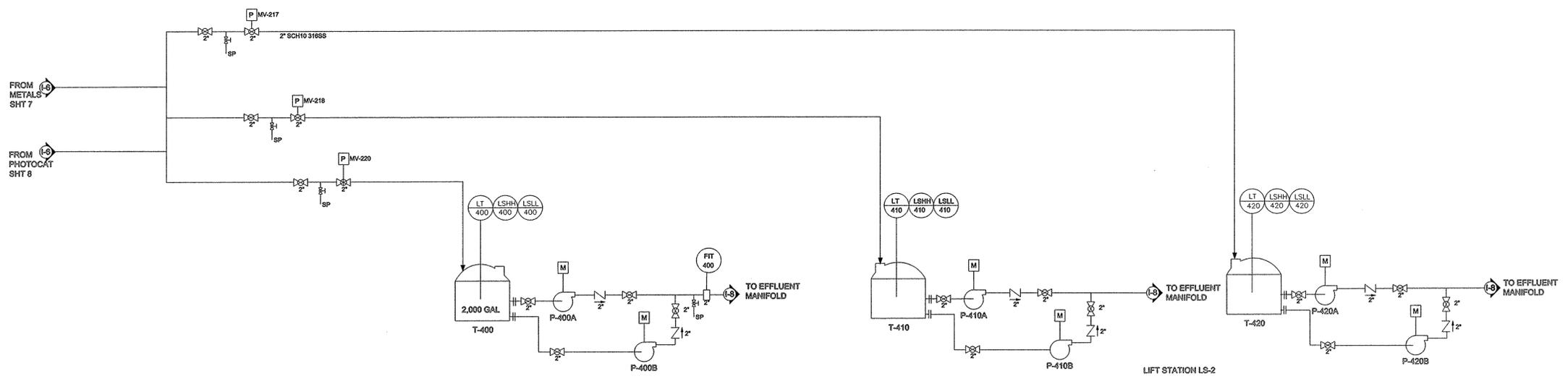
**MECHANICAL TREATMENT
PROCESS AND INSTRUMENTATION DIAGRAM**

SCALE NTS	DATE JUNE 28, 2013
PROJECT NO. 05-165 SEABOARD	AutoCAD 2010 PROCESS-FLOW-DIAGRAM.DWG

DRAWING NO.
1-5

REV. NO.
4

SHEET **5** OF **8**



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 Telephone: (205) 339-0689 Fax: (205) 339-4487

NO.	DATE	APPR.	REVISION	NO.	DATE	APPR.	REVISION
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1	5-18-10	S. Lucas	FOR BID PACKAGE SUBMITTAL				
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4	8-28-13		PER REQUESTED MODIFICATIONS				

**REMEDATION SYSTEM DESIGN DRAWINGS
 FORMER SEABOARD CHEMICAL FACILITY/
 RIVERDALE DRIVE LANDFILL SITE**

SEABOARD GROUP II JAMESTOWN, NC

DRAWN BY M. BROWN	PROJECT ENGINEER R. GLOVER
DESIGN ENGINEER S. LUCAS	PROJECT MANAGER J. LARUE

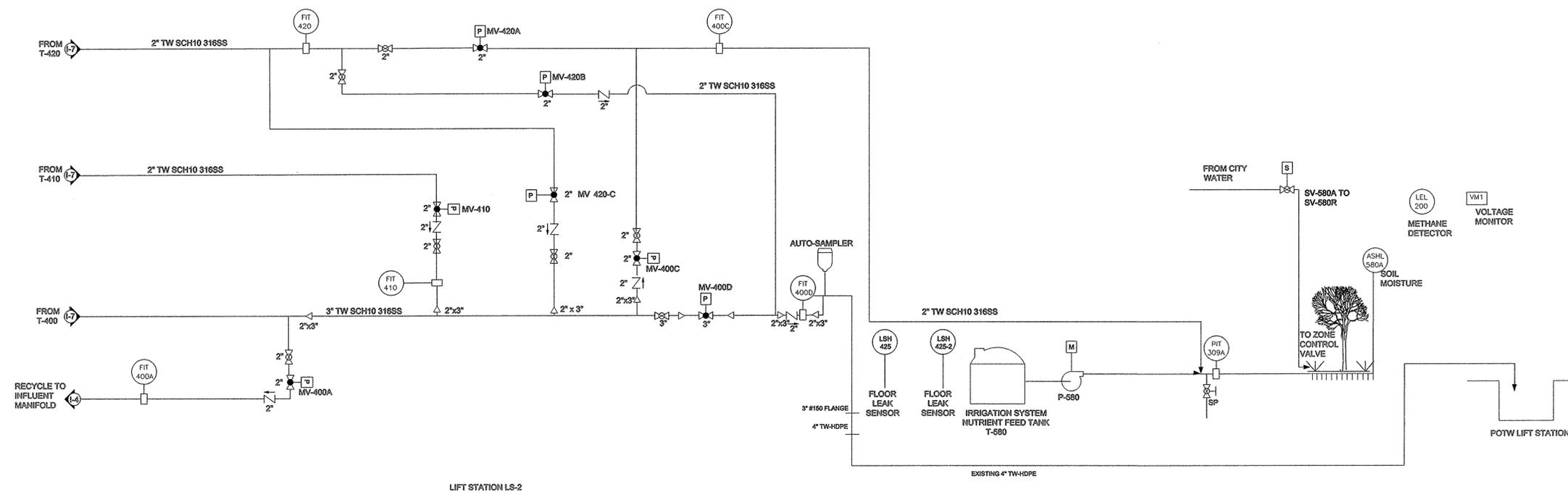
**MECHANICAL TREATMENT
 PROCESS AND INSTRUMENTATION DIAGRAM**

SCALE NTS	DATE JUNE 28, 2013
PROJECT NO. 05-165 SEABOARD	AutoCAD 2010 PROCESS-FLOW-DIAGRAM.DWG

DRAWING NO.
I-7

REV. NO.
4

SHEET **7** OF **8**



LIFT STATION LS-2

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CHEMTECH ENGINEERING, INC.
11254 SUNSET BAY NORTHPORT, ALABAMA 35475
Telephone: (205) 339-0689 Fax: (205) 339-4487

NO.	DATE	APPR.	REVISION	NO.	DATE	APPR.	REVISION
0	12-14-09	S. Lucas	FOR CLIENT REVIEW				
1	5-18-10	S. Lucas	FOR BID PACKAGE SUBMITTAL				
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3	9-20-12		PER INSTALLATION				
4	9-28-13		PER REQUESTED MODIFICATIONS				

**REMEDATION SYSTEM DESIGN DRAWINGS
FORMER SEABOARD CHEMICAL FACILITY/
RIVERDALE DRIVE LANDFILL SITE**

SEABOARD GROUP II JAMESTOWN, NC

DRAWN BY M. BROWN	PROJECT ENGINEER R. GLOVER
DESIGN ENGINEER S. LUCAS	PROJECT MANAGER J. LARUE

**MECHANICAL TREATMENT
PROCESS AND INSTRUMENTATION DIAGRAM**

SCALE NTS	DATE JUNE 28, 2013
PROJECT NO. 05-185 SEABOARD	AutoCAD 2010 PROCESS-FLOW-DIAGRAM.DWG

DRAWING NO.
1-8

REV. NO.
4

SHEET **8** OF **8**